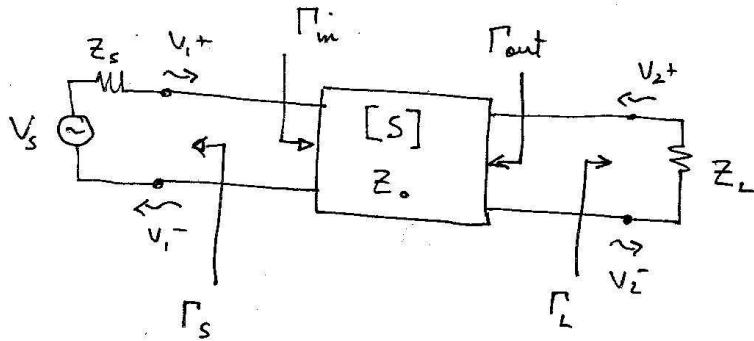


Transistor Amplifier - Power Gain Eqns.



Usando como referencia Z_0 , $\Gamma_s = \frac{Z_s - Z_0}{Z_s + Z_0}$, $\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$

Sabemos que: $V_1^- = S_{11}V_1^+ + S_{12}V_2^+$,
 $V_2^- = S_{21}V_1^+ + S_{22}V_2^+$

pero $\Gamma_{in} = \frac{V_1^-}{V_1^+}$

De aquí,

$$V_1^- = S_{11}V_1^+ + S_{12}\Gamma_L V_2^- \quad (*)$$

$$V_2^- = S_{21}V_1^+ + S_{22}\Gamma_L V_2^-$$

$$\rightarrow V_2^- = \frac{S_{21}V_1^+}{1 - S_{22}\Gamma_L}$$

$\Gamma_L = \frac{V_2^-}{V_2^+}$

Sustituyendo en (*)

$$V_1^- = S_{11}V_1^+ + S_{12}\Gamma_L \left(\frac{S_{21}V_1^+}{1 - S_{22}\Gamma_L} \right) \quad \text{Eg. en términos de } V_1^+ \text{ y } V_1^-$$

de aquí

$$\Gamma_{in} = \frac{V_1^-}{V_1^+} = S_{11} + \frac{S_{12}S_{21}\Gamma_L}{1 - S_{22}\Gamma_L} = \frac{Z_{in} - Z_0}{Z_{in} + Z_0} \quad (1)$$

De la misma forma,

$$\Gamma_{out} = \frac{V_2^-}{V_2^+} = S_{22} + \frac{S_{12}S_{21}\Gamma_s}{1 - S_{11}\Gamma_s} \quad (2)$$

Desarrollar expresión de potencia que entra a la red. 2

$$P_{in} = \frac{|V_1^+|^2}{2Z_0} (1 - |\Gamma_{in}|^2)$$

Hallar expresión para V_1^+ ;

$$V_1 = \frac{V_s Z_{in}}{Z_s + Z_{in}} = V_1^+ + V_1^- = V_1^+ (1 + \Gamma_{in})$$

$$V_1^+ = \frac{V_s Z_{in}}{(Z_s + Z_{in})(1 + \Gamma_{in})}, \text{ pero } Z_{in} = Z_0 \frac{1 + \Gamma_{in}}{1 - \Gamma_{in}}$$

$$\therefore V_1^+ = \frac{V_s \frac{1 + \Gamma_{in}}{1 - \Gamma_{in}} Z_0}{(Z_s + Z_{in})(1 + \Gamma_{in})} = \frac{V_s Z_0}{(Z_s + Z_0)(1 - \Gamma_{in})}$$

$$V_1^+ = \frac{V_s Z_0}{Z_0 \left(\frac{1 + \Gamma_s}{1 - \Gamma_s} + \frac{1 + \Gamma_{in}}{1 - \Gamma_{in}} \right) (1 - \Gamma_{in})} = \frac{V_s (1 - \Gamma_s)}{2 (1 - \Gamma_s \Gamma_{in})}$$

$$P_{in} = \frac{|V_s|^2 |1 - \Gamma_s|^2}{8 Z_0 |1 - \Gamma_s \Gamma_{in}|^2} (1 - |\Gamma_{in}|^2)$$

De la misma forma,

$$P_L = \frac{|V_2^-|^2}{2Z_0} (1 - |\Gamma_L|^2)$$

$$P_L = \frac{|V_s|^2 |S_{21}|^2 (1 - |\Gamma_L|^2) |1 - \Gamma_s|^2}{8 Z_0 |1 - S_{22} \Gamma_L|^2 |1 - \Gamma_s \Gamma_{in}|^2}$$

Definimos "Power Gain" 3

$$G = \frac{P_L}{P_{in}} = \frac{|S_{21}|^2 (1 - |\Gamma_L|^2)}{(1 - |\Gamma_{in}|^2) |1 - S_{22}\Gamma_L|^2}$$

Depende de

Γ_L

Eg. 11.8

"Available Gain", G_A

$$G_A = \frac{P_{AVN}}{P_{AVS}} ; \quad P_{AVN} = P_L \Big|_{\Gamma_L = \Gamma_{out}^*}$$

$$P_{AVS} = P_{in} \Big|_{\Gamma_{in} = \Gamma_S^*}$$

$$P_{AVS} = \frac{|V_S|^2}{8Z_0} \frac{|1 - \Gamma_S|^2}{|1 - |\Gamma_S|^2|^2} \left(\cancel{1 - |\Gamma_S|^2} \right) = \frac{|V_S|^2}{8Z_0} \frac{|1 - \Gamma_S|^2}{|1 - |\Gamma_S|^2|^2}$$

$$P_{AVN} = \frac{|V_S|^2}{8Z_0} \frac{|S_{21}|^2 (1 - |\Gamma_{out}|^2) |1 - \Gamma_S|^2}{|1 - S_{22}\Gamma_{out}^*| |1 - \Gamma_S\Gamma_{in}|^2}$$

pero $\Gamma_{in} = S_{11} + \frac{S_{12}S_{21}\Gamma_L}{1 - S_{22}\Gamma_L} = S_{11} + \frac{S_{12}S_{21}\Gamma_{out}^*}{1 - S_{22}\Gamma_{out}^*}$

$$P_{AVN} = \frac{|V_S|^2}{8Z_0} \frac{|S_{21}|^2 |1 - \Gamma_S|^2}{|1 - S_{11}\Gamma_S|^2 (1 - |\Gamma_{out}|^2)}$$

$$G_A = \frac{P_{AVN}}{P_{AVS}} = \frac{|S_{21}|^2 (1 - |\Gamma_S|^2)}{|1 - S_{11}\Gamma_S|^2 (1 - |\Gamma_{out}|^2)}$$

Depende de

Γ_S

Eg. 11.12

Transducer Power Gain

$$G_T = \frac{P_L}{P_{Avs}} = \frac{|S_{21}|^2 (1 - |\Gamma_S|^2) (1 - |\Gamma_L|^2)}{|1 - \Gamma_S \Gamma_{in}|^2 |1 - S_{22} \Gamma_L|^2}$$

Depende
de Γ_S y Γ_L
Eq. 11.13

Si $\Gamma_L = \Gamma_S = 0$ $G_T = |S_{21}|^2$

Caso especial \Rightarrow caso unilateral $\Rightarrow S_{12} = 0$

Si $S_{12} = 0$ entonces $\Gamma_{in} = S_{11}$ (eq. 1), $\Gamma_{out} = S_{22}$ (eq. 2)
y G_T se reduce a

$$G_{Tu} = \frac{|S_{21}|^2 (1 - |\Gamma_S|^2) (1 - |\Gamma_L|^2)}{|1 - S_{11} \Gamma_S|^2 |1 - S_{22} \Gamma_L|^2}$$

Ejemplo: $S_{11} = 0.45 \angle 150^\circ$ $S_{12} = 0.01 \angle -10^\circ$
 $S_{21} = 2.05 \angle 10^\circ$ $S_{22} = 0.4 \angle -150^\circ$

Si $Z_S = 20 \Omega$ y $Z_L = 30 \Omega$
 $\Gamma_S = -0.429$; $\Gamma_L = -0.250$

De aqui: $\Gamma_{in} = S_{11} + \frac{S_{12} S_{21} \Gamma_L}{1 - S_{22} \Gamma_L} = 0.455 \angle 150^\circ$
 $\Gamma_{out} = 0.408 \angle -151^\circ$

$G = 5.94$ $G_A = 5.85$ $G_T = 5.49$

Podemos Dividir ganancia en tres términos :

$$G_T = G_S G_0 G_L$$

$$\text{Donde } G_S = \frac{1 - |\Gamma_S|^2}{|1 - \Gamma_S \Gamma_{in}|^2}; \quad G_0 = |S_{21}|^2; \quad G_L = \frac{1 - |\Gamma_L|^2}{|1 - S_{22} \Gamma_L|^2}$$

$G_S \Rightarrow$ Input Matching Network

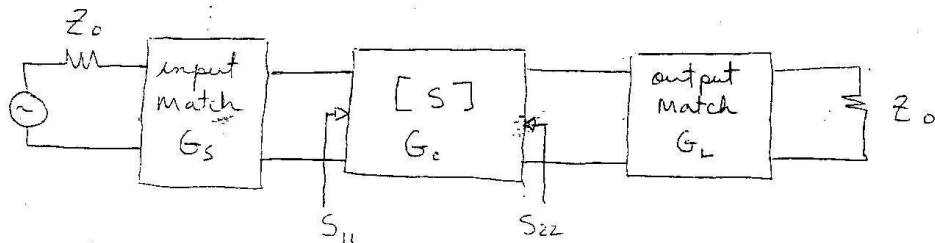
$G_L \Rightarrow$ output " "

$G_0 \Rightarrow$ transistor (S_{21})

Caso especial (unilateral) existe si $S_{12} = 0$

De esta condición : $\Gamma_{in} = S_{11}$; $\Gamma_{out} = S_{22}$

$$G_{TU} = \frac{|S_{21}|^2 (1 - |\Gamma_S|^2) (1 - |\Gamma_L|^2)}{|1 - S_{11} \Gamma_S|^2 |1 - S_{22} \Gamma_L|^2}$$



$$G_S = \frac{1 - |\Gamma_S|^2}{|1 - S_{11} \Gamma_S|^2} \quad G_0 = |S_{21}|^2 \quad G_L = \frac{1 - |\Gamma_L|^2}{|1 - S_{22} \Gamma_L|^2}$$

Proximo Tema: Estabilidad

Estabilidad: El amplificador es estable si $|\Gamma_{in}| < 1$ y $|\Gamma_{out}| < 1$. Γ_{in} y Γ_{out} dependen de Γ_s y Γ_L , por lo que Γ_s y Γ_L controlan la estabilidad del amplificador.

Deseamos valores de Γ_L y Γ_s para que Γ_{in} y Γ_{out} resulten < 1 . Habran valores que ocasionen: $|\Gamma_{in}| > 1$ $|\Gamma_{out}| > 1$ } inestable

Usando las ecuaciones de Γ_{in} y Γ_{out} , podemos derivar expresiones para identificar valores de Γ_L y Γ_s deseados; usando el

"Smith Chart". Hay dos tipos:

1) Estabilidad sin condicion: $|\Gamma_{in}|$ y $|\Gamma_{out}|$ son < 1 para cualquier Γ_L y Γ_s .

2) Estabilidad condicional $|\Gamma_{in}|$ y $|\Gamma_{out}| < 1$ para algunos valores de Γ_L y Γ_s . ¿Cómo identifico estos valores?

$|\Gamma_{in}| = 1$ $|\Gamma_{out}| = 1$ podemos
 determinar valores de Γ_S y Γ_L donde esto
 se cumple.

$$|\Gamma_{in}| = \left| S_{11} + \frac{S_{12} S_{21} \Gamma_L}{1 - S_{22} \Gamma_L} \right| = 1$$

$$|\Gamma_{out}| = \left| S_{22} + \frac{S_{12} S_{21} \Gamma_S}{1 - S_{11} \Gamma_S} \right| = 1$$

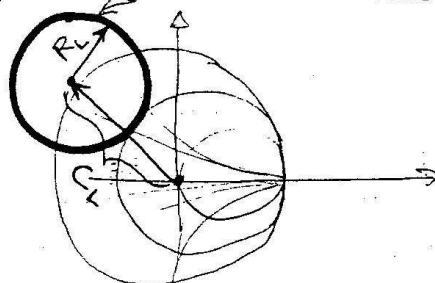
De aquí resulta ecuaciones de círculo

Centro Radio

$$C_L = \frac{(S_{22} - \Delta S_{11}^*)^*}{|S_{22}|^2 - |\Delta|^2} \quad R_L = \left| \frac{S_{12} S_{21}}{|S_{22}|^2 - |\Delta|^2} \right|$$

En plano de Γ_L sobre el círculo: $|\Gamma_{in}| = 1$

"Output Stability
 circle"

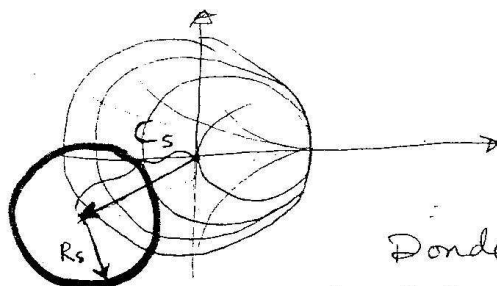


En plano de Γ_S

"Input Stability
 circle"

$$C_S = \frac{(S_{11} - \Delta S_{22}^*)^*}{|S_{11}|^2 - |\Delta|^2}$$

$$R_S = \left| \frac{S_{12} S_{21}}{|S_{11}|^2 - |\Delta|^2} \right|$$



Donde:

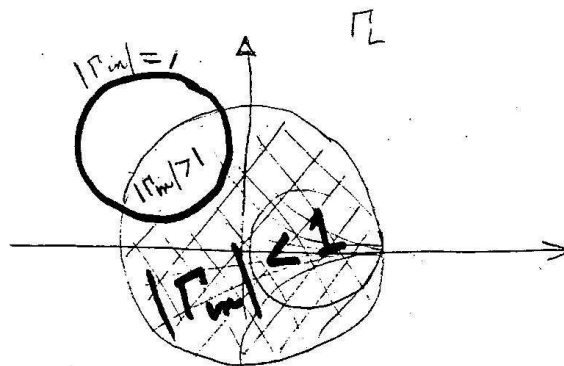
$$\Delta = S_{11} S_{22} - S_{12} S_{21}$$

¿ Como Determine si region estable es dentro o fuera del círculo?

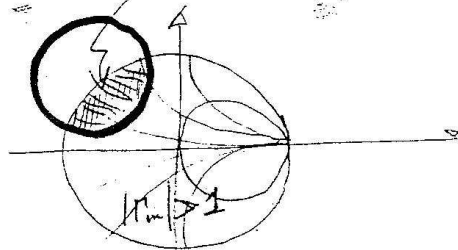
Usar punto facil : $\Gamma_L = 0$ (centro del S.C.)

$$\therefore |\Gamma_{in}| = \left| S_{11} + \frac{S_{12} S_{21} \Gamma_L}{1 - S_{22} \Gamma_L} \right| = |S_{11}|$$

Si $|S_{11}| < 1$, la region que contiene el centro del S.C. es estable

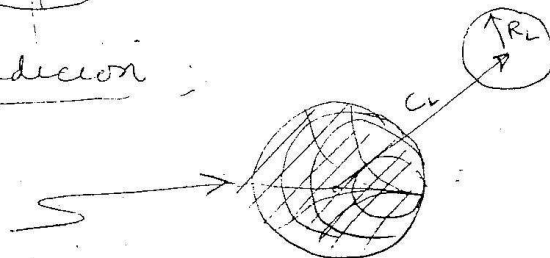


Si $|S_{11}| > 1$ $|\Gamma_{in}| < 1$ (Region estable)

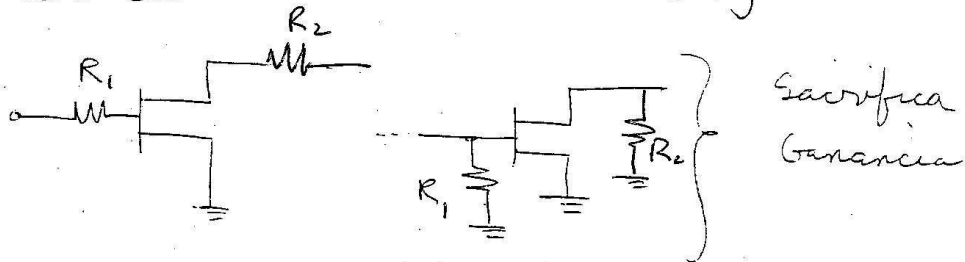


Estable Sin Condicion :

Todo Γ_L
resulta en
 $|\Gamma_{in}| < 1$



si el transistor es estable con condicion, 6
 podemos cambiar esta condicion a estable
sin condicion con "resistive loading"



Usar uno de los dos (R_1, R_2)

Diseño de Amplificador (Ganancia Maxima)

$$\Gamma_{in} = \Gamma_S^* \quad (\text{Maxima transferencia en entrada de amplificador})$$

$$\Gamma_{out} = \Gamma_L^* \quad (\text{Maxima transferencia en salida del amplificador})$$

$$G_{Tmax} = \frac{1}{1 - |\Gamma_S|^2} |S_{21}|^2 \frac{1 - |\Gamma_L|^2}{|1 - S_{22}\Gamma_L|^2}$$

$$\Gamma_{in} = \Gamma_S^* = S_{11} + \frac{S_{12}\Gamma_L S_{21}}{1 - S_{22}\Gamma_L}$$

$$\Gamma_{out} = \Gamma_L^* = S_{22} + \frac{S_{12}S_{21}\Gamma_S}{1 - S_{11}\Gamma_S}$$

Doz ecuaciones
 desordenadas!
 Γ_L y Γ_S

De aquí resulta que:

7

$$\Gamma_S = \frac{B_1 \pm \sqrt{B_1^2 - 4|C_1|^2}}{2C_1}$$

$$\Gamma_L = \frac{B_2 \pm \sqrt{B_2^2 - 4|C_2|^2}}{2C_2}$$

Donde $B_1 = 1 + |S_{11}|^2 - |S_{22}|^2 - |\Delta|^2$

$$B_2 = 1 + |S_{22}|^2 - |S_{11}|^2 - |\Delta|^2$$

$$C_1 = S_{11} - \Delta S_{22}^*$$

$$C_2 = S_{22} - \Delta S_{11}^*$$

Para caso unilateral;

$$\Gamma_S = S_{11}^* \quad \Gamma_L = S_{22}^*$$

$$G_{TU \max} = \frac{1}{1 - |S_{11}|^2} |S_{21}|^2 \frac{1}{1 - |S_{22}|^2}$$

Otras condiciones matemáticas de estabilidad

Estable sin condición:

$$K = \frac{1 - |S_{11}|^2 - |S_{22}|^2 + |\Delta|^2}{2|S_{12}S_{21}|} > 1$$

$$M = \frac{1 - |S_{11}|^2}{|S_{22} - S_{11}^* \Delta| + |S_{21}S_{12}|} > 1$$

$$\text{y } |\Delta| < 1$$