

Ruido en sistemas de microondas

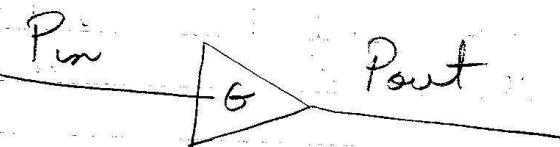
(movimiento de electrones en conductores)

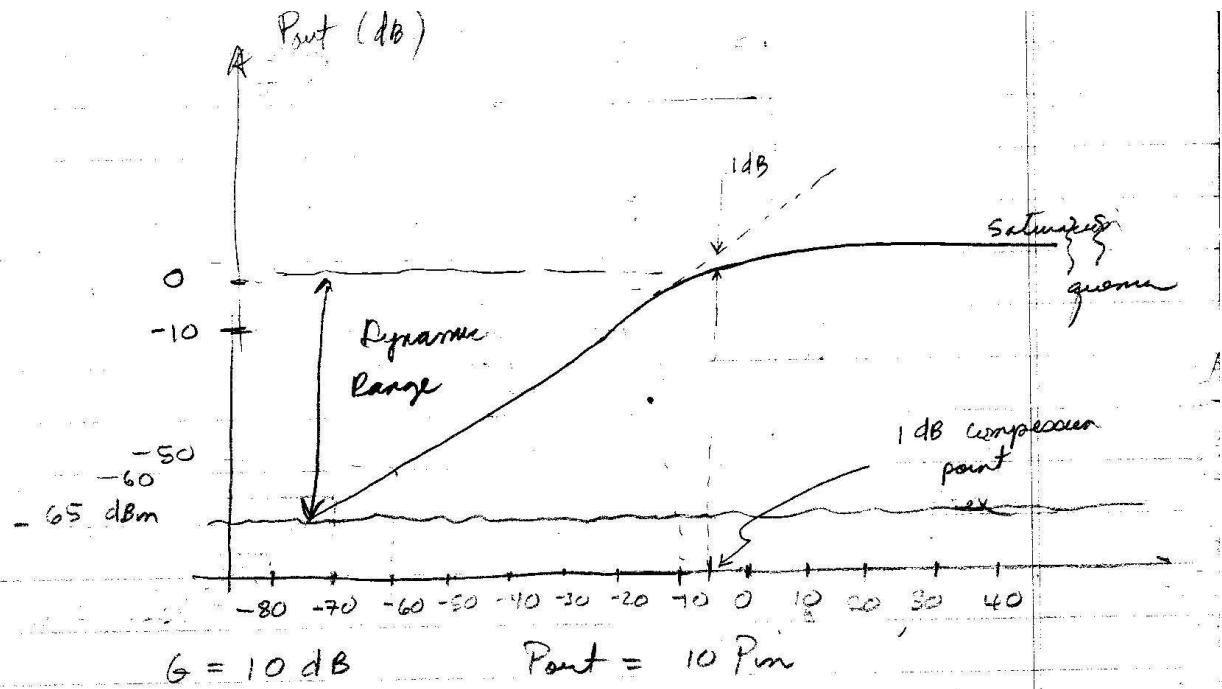
→ se puede generar fuera o dentro del sistema

nivel de ruido → límite de energía mínima que se puede detectar

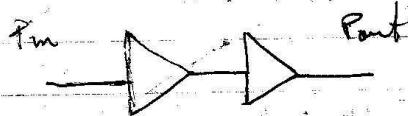
→ deseamos minimizar ruido

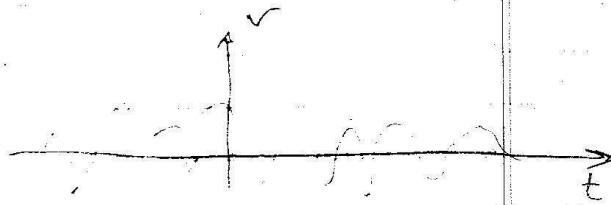
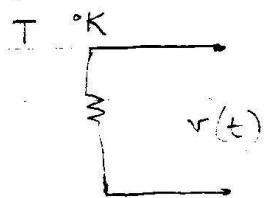
→ radiometro → distingue entre el potencia de ruido recibida y la generada en el sistema.





$1 \text{ dB C.P.} \rightarrow \text{Pout está } 1 \text{ dB por debajo de amplificador ideal}$





$$\langle v \rangle = 0 \quad \langle v_n \rangle = v_n \neq 0$$

Para microondas:

$$v_n = \sqrt{4kTBR} \quad \leftarrow \text{no depende de } f \text{ ("white noise")}$$

$k \rightarrow$  constante Boltzmann  $= 1.380 \times 10^{-23} \text{ J/K}$

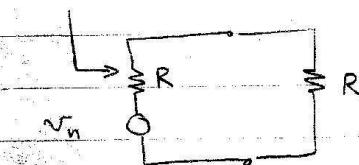
$T \rightarrow$  Temperatura ( $^{\circ}\text{K}$ )

$B \rightarrow$  ancho de banda del sistema [Hz]

$R \rightarrow$  Resistencia ( $\Omega$ )

Modelo:

no ruido



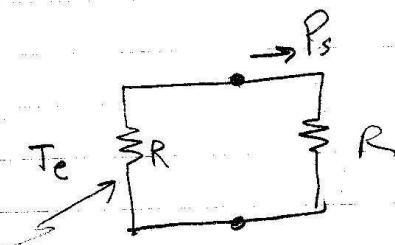
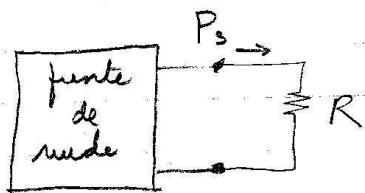
Potencia de ruido

$$P_n = \chi^2 R = \left( \frac{v_n}{2R} \right)^2 R$$

$$= \frac{v_n^2}{4R} = \frac{4kTBR}{4R} = kTB$$

$B \rightarrow 0$        $P_n \rightarrow 0$  (Recege menos níide)  
 $T \rightarrow 0$        $P_n \rightarrow 0$  (no tiene níide)  
 $B \rightarrow \infty$        $P_n \rightarrow \infty$  (no existe)  
 eq. no vale de

Potencia de níide (termal) se  
 puede modelar con temperatura  
 equivalente de níide ( $T_e$ )



$T_e \rightarrow$  temperatura que produce misma  
 potencia ( $P_s$ ) generada por fuente de  
 níide

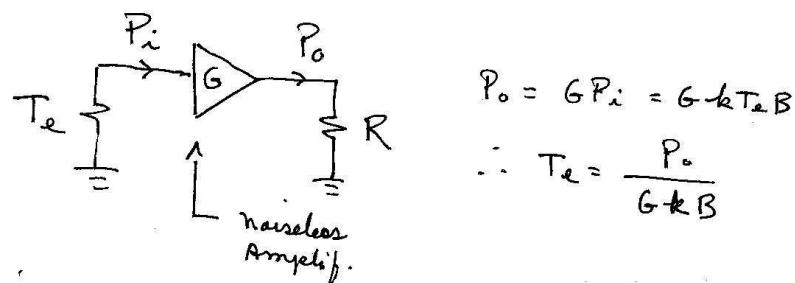
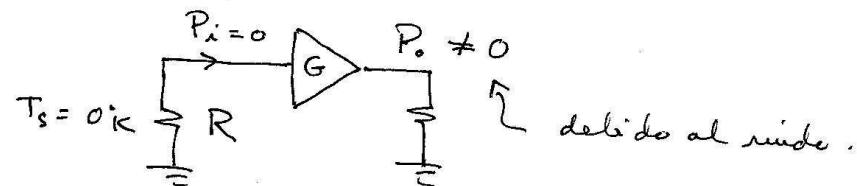
$$P = kTB$$

$$P_s = kT_e B \Rightarrow T_e = \frac{P_s}{kB}$$

se clase, potencia de ruido  $P_n = kTB$ .

El ruido que se genera en un amplificador lo podemos caracterizar con  $T_e$ , temperatura equivalente de ruido:

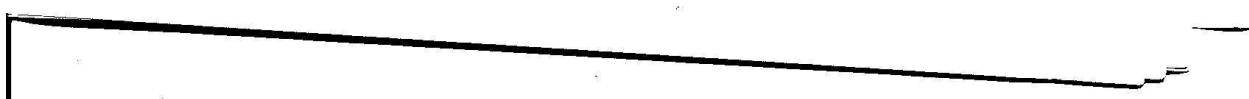
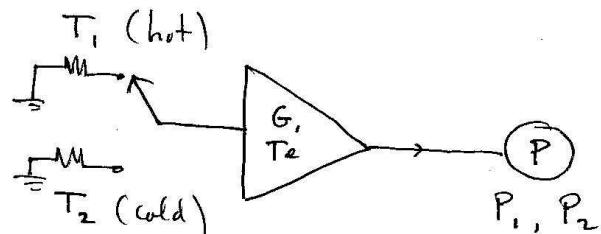
Así derán:



Ruido en amplificador se representa con  $T_e$ .



Método "factor -γ" para medir  $T_e$  del amplificador



$$P_2 = kT_2 BG + kT_e BG$$

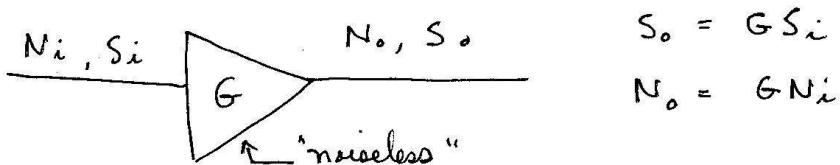
$$\gamma = \frac{P_1}{P_2} = \frac{T_1 + T_e}{T_2 + T_e} \implies P_1 \text{ y } P_2 \text{ son medidas} \therefore \text{cong } \gamma.$$

$$\gamma(T_2 + T_e) = T_1 + T_e \implies T_e = \frac{T_1 - \gamma T_2}{(\gamma - 1)}$$

Figura de ruido ("Noise Figure") - F → medida que caracteriza ruido en componentes (amplificadores, sistemas, subsistemas, etc...). Compara ruido entre entrada y salida del sistema.

$$\frac{S_i/N_i}{S_o/N_o} \geq 1$$

S/N → "signal-to-noise" ratio ⇒ razón de señal deseable (S) entre potencia de ruido (N)



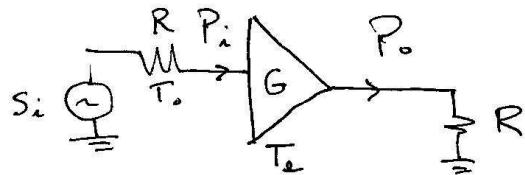
$$S_o = GS_i$$

$$N_o = GN_i$$

$$F = \frac{S_i/N_i}{S_o/N_o} = \frac{S_i/N_i}{GS_i/GN_i} = 1 \quad \text{No noise!}$$

$$F = \frac{G S_i}{G N_i + \Delta N} > 1 \quad \underline{\text{noisy}} !$$

Para medir  $F$ , usaremos por definición  $N_i = k T_0 B$   
 $T_0 = 290^\circ \text{K}$



$$P_i = N_i + S_i ; \quad P_o = N_o + S_o$$

$$P_o = GS_i + \underbrace{GN_i + GkT_e B}_{N_o}$$

$$\Rightarrow N_o = GN_i + GkT_e B = GkT_0 B + GkT_e B$$

$$N_o = GkB(T_0 + T_e)$$

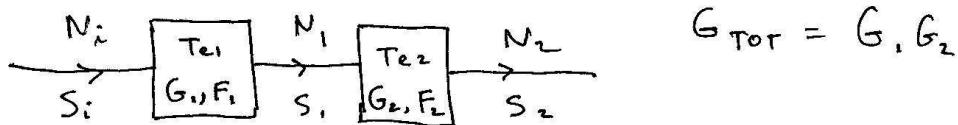
$$F = \frac{S_i/N_i}{S_o/N_o} = \frac{S_i}{N_i} \cdot \frac{N_o}{S_o} = \frac{S_i}{kT_0 B} \cdot \frac{GkB(T_0 + T_e)}{GS_i}$$

$$F = \frac{T_0 + T_e}{T_0} = 1 + \frac{T_e}{T_0}$$

$$F = 1 + \frac{T_e}{T_0}$$

$$T_e = (F - 1)T_0$$

Cascade configuration:



$$N_2 = G_{TOT} \frac{1}{k} B T_0 + G_{TOT} \frac{1}{k} B T_{cas}. \quad (1)$$

$$N_1 = G_1 \frac{1}{k} T_0 B + G_1 \frac{1}{k} T_{e1} B$$

$$N_2 = N_1 G_2 + G_2 \frac{1}{k} T_{e2} B$$

$$\begin{aligned} &= G_1 G_2 \frac{1}{k} T_0 B + G_1 G_2 \frac{1}{k} T_{e1} B + G_2 \frac{1}{k} T_{e2} B \\ &= G_1 G_2 \frac{1}{k} B \left( T_0 + T_{e1} + \frac{T_{e2}}{G_1} \right) \end{aligned}$$

Comparando con (1):

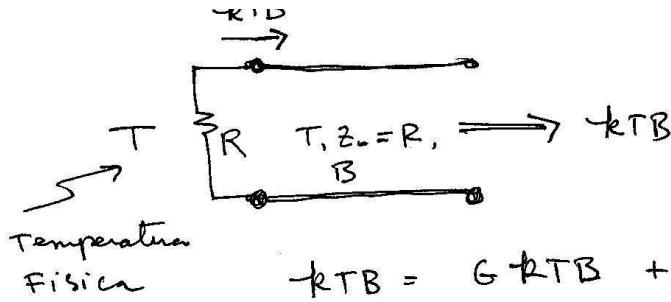
$$T_{cas} = T_{e1} + \frac{T_{e2}}{G_1}$$

$$F_{cas} = 1 + \frac{T_{cas}}{T_0} = F_1 + \frac{(F_2 - 1)}{G_1}$$

En general:

$$T_{cas} = T_{e1} + \frac{T_{e2}}{G_1} + \frac{T_{e3}}{G_1 G_2} + \dots$$

$$F_{cas} = F_1 + \frac{F_2 - 1}{G_1} + \frac{F_3 - 1}{G_1 G_2} + \dots$$



$$-kTB = G \cdot kTB + G \cdot N_{\text{add}}$$

$$G \rightarrow \text{losses} \rightarrow G < 1 \rightarrow L = \frac{1}{G}$$

$$\therefore G < 1 ; \quad L > 1$$

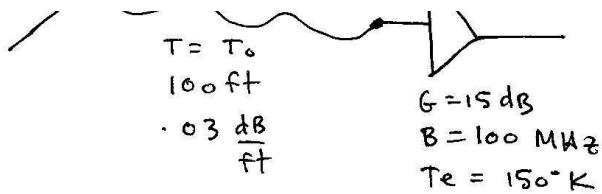
$$N_{\text{add}} = \frac{-kTB (1-G)}{G} = -kT_e B$$

$$T_e = \frac{T(1-G)}{G} = T(L-1)$$

$$\text{Since } F = 1 + \frac{T_e}{T_0} \Rightarrow F = 1 + \frac{T}{T_0} (L-1)$$

$$\text{Si } T = T_0 \Rightarrow F = L$$

Por ejemplo: un atenuador de 3 dB a  $T = T_0$   
tiene Figura de ruido  $F = 3 \text{ dB}$



$$F_{\text{cas}} = F_1 + \frac{F_2 - 1}{G_1}$$

a) Since  $T = T_0 \Rightarrow F_1 = \text{attenuation}$

$$\text{Attenuation} = \cdot 0.3 \frac{\text{dB}}{\text{ft}} \cdot 100 = 3 \text{ dB}$$

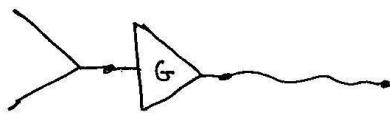
$$F_1 = 3 \text{ dB} \Rightarrow G_1 = 0.5 ; L = 2$$

$$F_1 = 1 + \frac{T}{T_0} (L-1) = 1 + \frac{150}{290} (2-1) = 2$$

$$F_{\text{amp}} = 1 + \frac{T_e}{T_0} = 1 + \frac{150}{290} = 1.52$$

b)

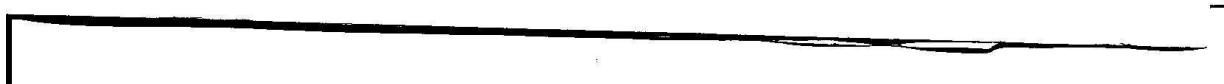
$$F_{\text{cas}} = 2 + \frac{1.52 - 1}{0.5} = 3.04 = \underline{4.82 \text{ dB}}$$



$$F_{\text{cas}} = 1.52 + \frac{2-1}{31.62} = 1.55$$

$$G = 15 \text{ dB} \Rightarrow 10^{1.5} = 31.62 = 1.9 \text{ dB}$$

$$\text{From } F_a = 4.82 \text{ dB} \Rightarrow F_b = \underline{\underline{1.9 \text{ dB}}}$$



$$BW = 150 \times 10^6 \text{ Hz}$$

$$F = 4 \text{ dB} = 2.51$$

$$F_{\text{caac}} = F_1 + \frac{F_2 - 1}{G_1} = 2.51 + \frac{4.10 - 1}{15.8}$$

10.7

$$T_e = \frac{P_s}{k_B} = \frac{(10^{-85/10})(10^{-3})}{(1.38 \times 10^{-23})(1 \times 10^9)} = 229 \text{ K}$$

$$= 2.71 = 4.3 \text{ dB}$$

$$F_{\text{Amp}} = 1 + \frac{T_e}{T_0} = 1 + \frac{180}{290} = 1.62 = 2.1 \text{ dB}$$

$$F_{\text{line}} = 1 + (L-1) \frac{T}{T_0} = 1 + (1.41-1) \frac{300}{290} = 1.43 \quad L > 1$$

$$F_{\text{caac}} = F_1 + \frac{1}{G_1} (F_2 - 1) = F_1 + L(F_2 - 1) = 1.43 + (1.41)(1.62 - 1) = 2.3 = 3.6 \text{ dB}$$

$$P_{\text{noise}} = P_{\text{due input}} + P_{\text{due system}}$$

$$P_{\text{d. input}} = -85 \text{ dBm} - 1.5 \text{ dB} + 12 \text{ dB} = -74.5 \text{ dBm} = 3.55 \times 10^{-11} \quad G_{\text{cas}} = 12 - 1.5 \text{ dB} \\ = 10.5 \text{ dB}$$

$$P_{\text{d. system}} = k T_e B G_{\text{cas}} = k (F_{\text{caac}} - 1) T_0 B G_{\text{cas}} = k (2.3 - 1) (1 \times 10^9) (10^{10.5}) (290)$$

$$P_{\text{noise}} = 5.84 \times 10^{-11} + 3.55 \times 10^{-11} \text{ W} = 9.39 \times 10^{-11} \text{ W} = -70.3 \text{ dBm}$$

10.8

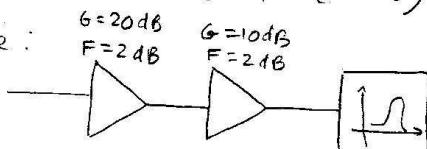
$$F_{\text{caac}} = F_1 + \frac{F_2 - 1}{G_1} + \frac{F_3 - 1}{G_1 G_2} = 1.41 + (1.41)(1.58 - 1) + \frac{1.41}{10} (1.58 \cdot 1) = 2.31 = 3.64 \text{ dB}$$

$$\cancel{P_{\text{in}}} = -90 \text{ dBm} \quad P_{\text{out}} = -90 - 1.5 + 10 + 20 = -61.5 \text{ dBm}$$

$$P_n = G_{\text{cas}} k T_{\text{cas}} B = k (F_{\text{caac}} - 1) T_0 B G_{\text{cas}} \\ = 1.38 \times 10^{-23} (2.31 - 1) (290) (10^8) (10^{28.5/10}) = 3.71 \times 10^{-10} \text{ W}$$

$$\left(\frac{S_o}{N_o}\right)_{\text{dB}} = S_o \text{ dB} - N_o \text{ dB} = -61.5 - (-64.3) = \underline{\underline{2.8 \text{ dB}}}$$

Best noise Figure:



$$F_{\text{caac}} = 1.59 + \frac{(1.59 - 1)}{100} + \frac{(1.41 - 1)}{1000} = 1.586 = \underline{\underline{2 \text{ dB}}}$$