

Review of Bipolar Junction Transistors

INEL 4207 Digital Electronics

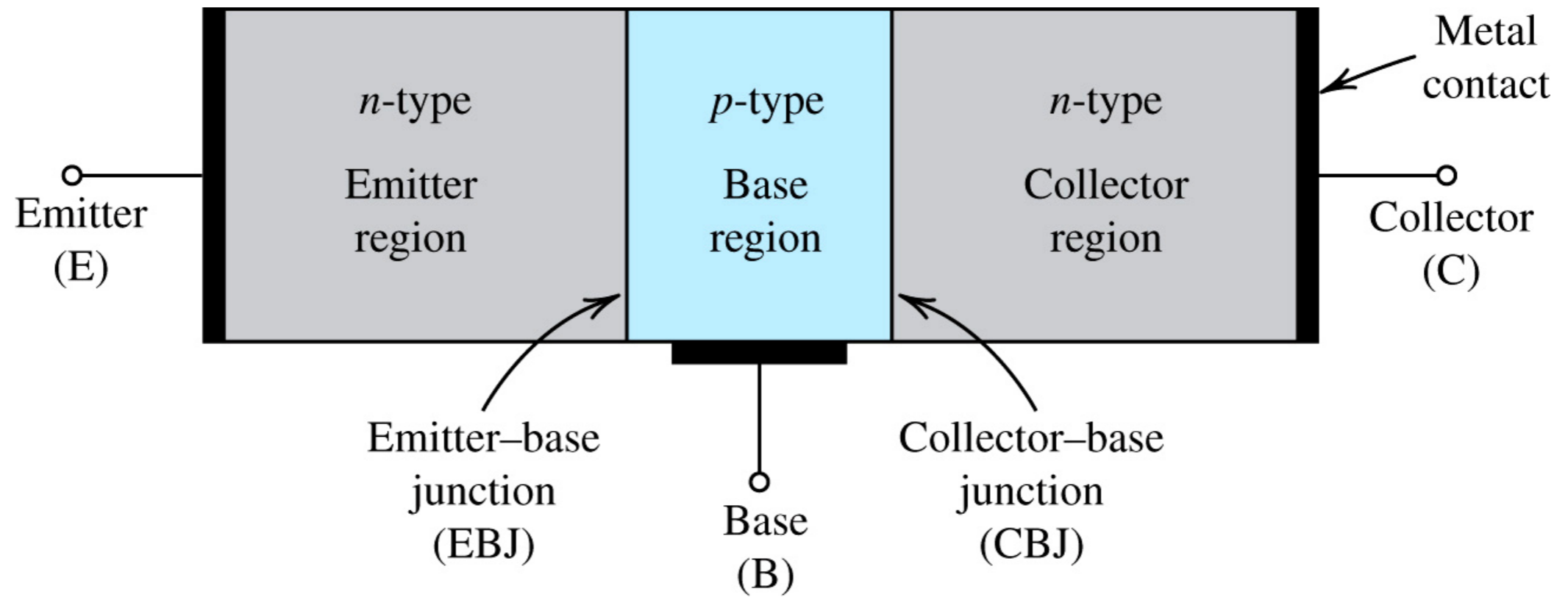
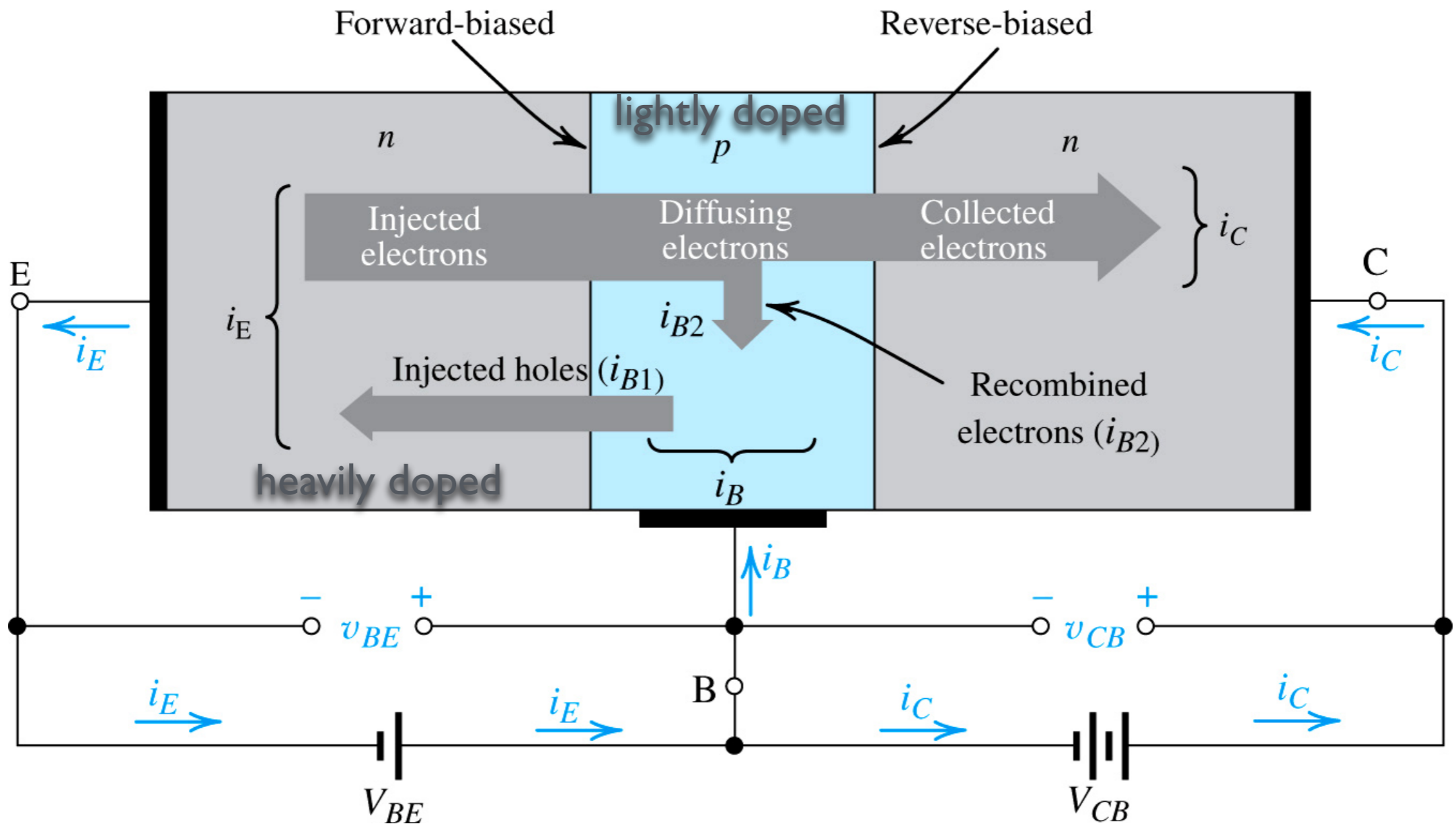


Figure 6.1: A simplified structure of the *npn* transistor.

Modes of operation

	EBJ	CBJ
Cutoff	Reverse	Reverse
Active	Forward	Reverse
Saturation	Forward	Forward



Current flow

- **emitter current (i_E)** – is current which flows across EBJ
 - Flows “out” of emitter lead
- **minority carriers** – in p -type region.
 - These electrons will be injected from emitter into base.
 - Opposite direction (in relation to conventional current).
- Because base is thin, concentration of excess minority carriers within it will exhibit constant gradient.

$n_p(x)$ = concentration of minority carriers at position x (where 0 represents EBJ boundary)
 n_{p0} = thermal-equilibrium value of minority carrier (electron) concentration in base region
 v_{BE} = voltage applied across base-emitter junction
 V_T = thermal voltage (constant)

$$(eq6.1) \quad n_p(0) = n_{p0} e^{v_{BE}/V_T}$$

Straight line represents constant gradient.

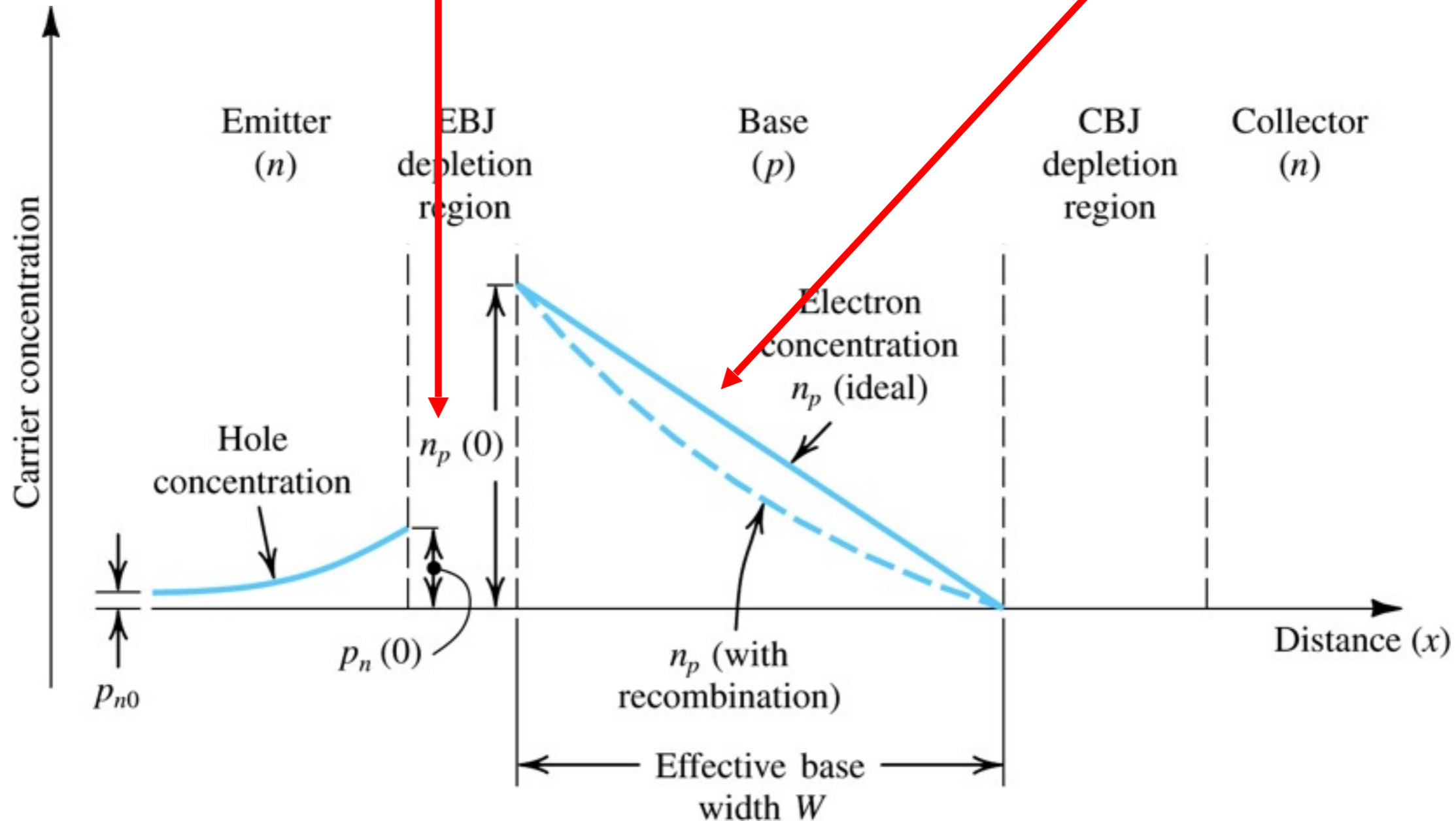


Figure 6.4 Profiles of minority-carrier concentrations in the base and in the emitter of an *npn* transistor operating in the active mode:
 $v_{BE} > 0$ and $v_{CB} \geq 0$.

Current Flow

- Tapered minority-carrier concentration profile exists.
- It causes electrons injected into base to diffuse through base toward collector.
- As such, electron diffusion current (I_n) exists.

A_E = cross-sectional area of the base-emitter junction
 q = magnitude of the electron charge
 D_n = electron diffusivity in base
 W = width of base

$$\text{(eq6.2)} \quad I_n = A_E q D_n \frac{dn_p(x)}{dx}$$

$$\text{(eq6.2)} \quad I_n = A_E q D_n \left(\frac{-dn_p(0)}{W} \right)$$

this simplification
may be made if
gradient assumed
to be straight line

Current Flow

- Some “diffusing” electrons **will combine with holes** (majority carriers in base).
- Base is thin, however, and **recombination is minimal**.
- Recombination does, however, **cause gradient to take slightly curved shape**.
 - The straight line is assumed.

BJT basic equations

$$i_C = I_S e^{v_{BE}/V_T}$$

$$I_S = \frac{A_E q D_n n_{p0}}{W} = \frac{A_E q D_n n_i^2}{N_A W}$$

$$\beta = \frac{i_C}{i_B} \Rightarrow i_B = \frac{I_S}{\beta} e^{v_{BE}/V_T}$$

$$i_E = i_C + i_B = (\beta + 1)i_B = \frac{\beta}{\beta + 1} i_C = \alpha i_C$$

$$\beta = \frac{\alpha}{1 - \alpha}$$

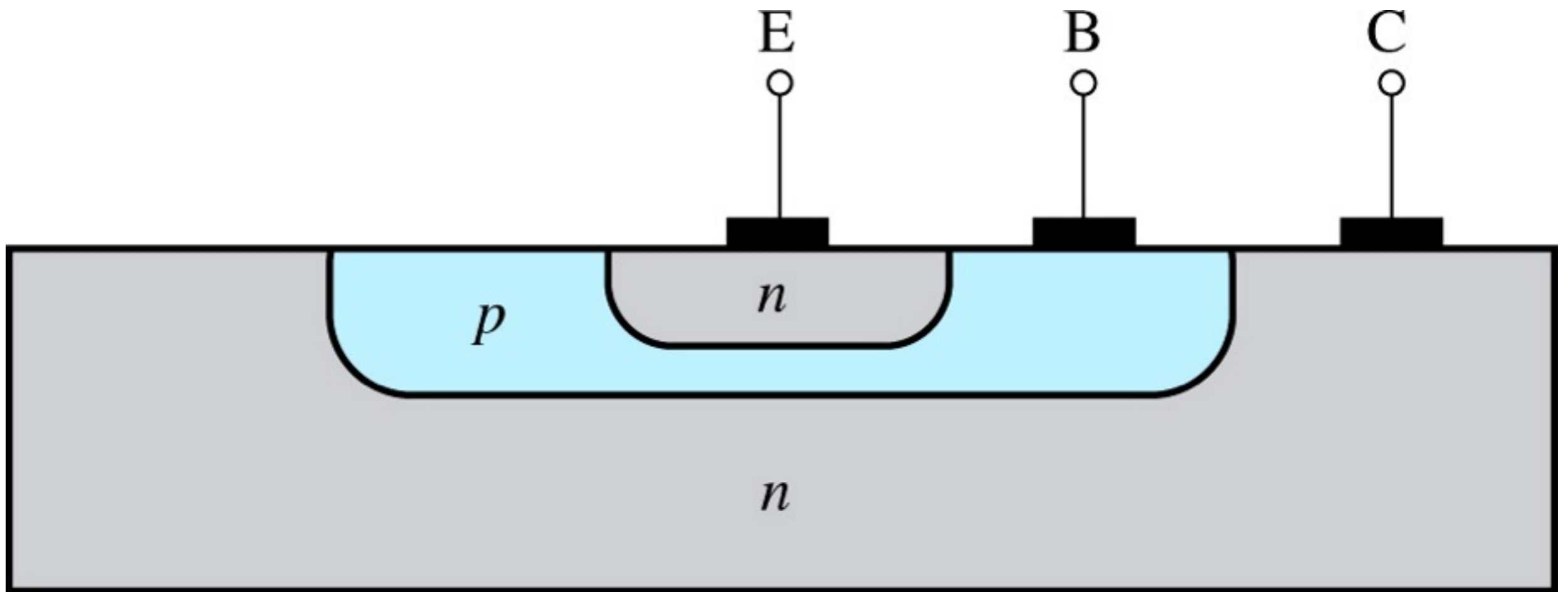


Figure 6.7: Cross-section of an *npn* BJT.

The *pn*p Transistor

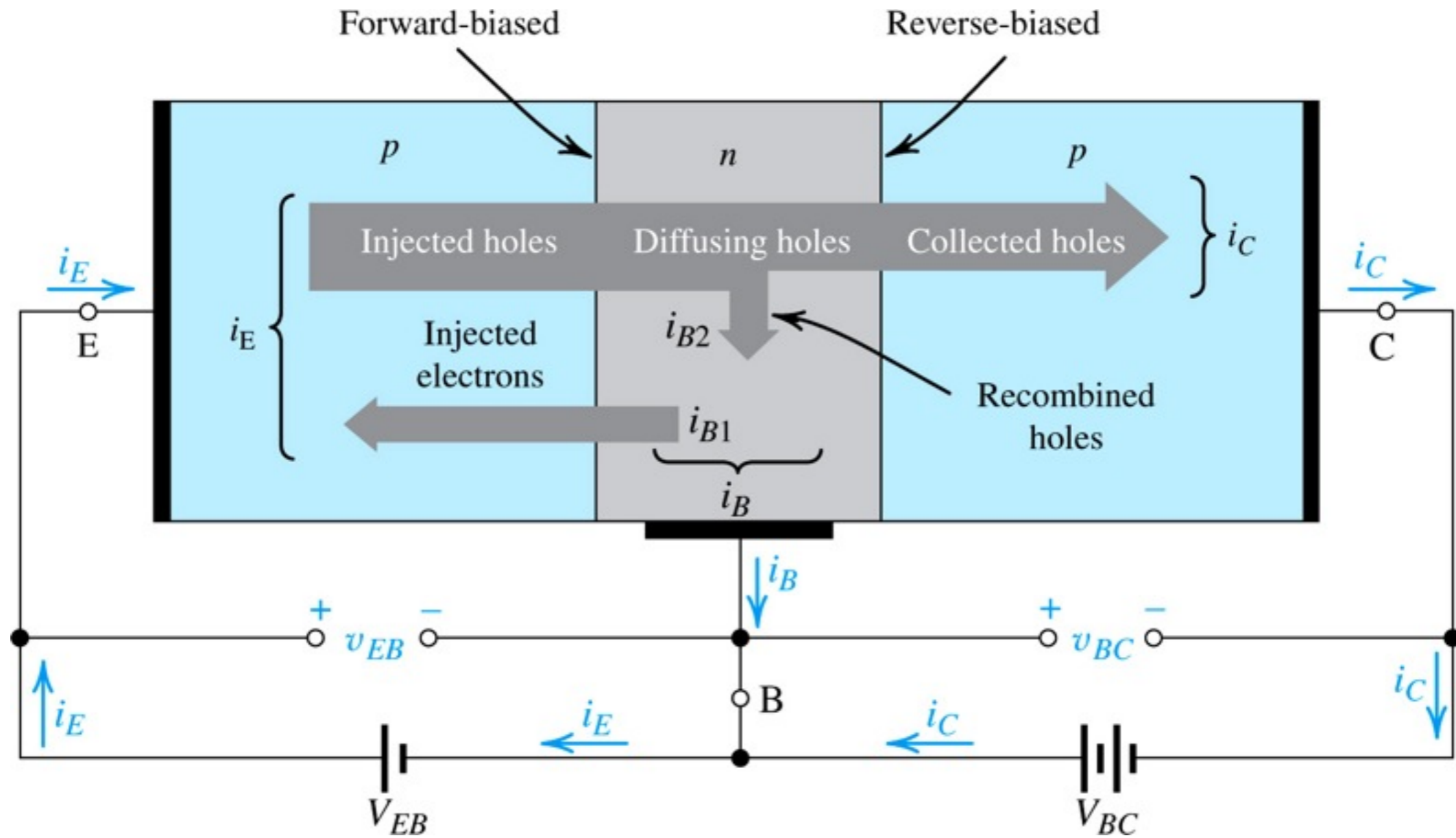


Figure 6.10: Current flow in a *pn*p transistor biased to operate in the active mode.

6.2. Current-Voltage Characteristics

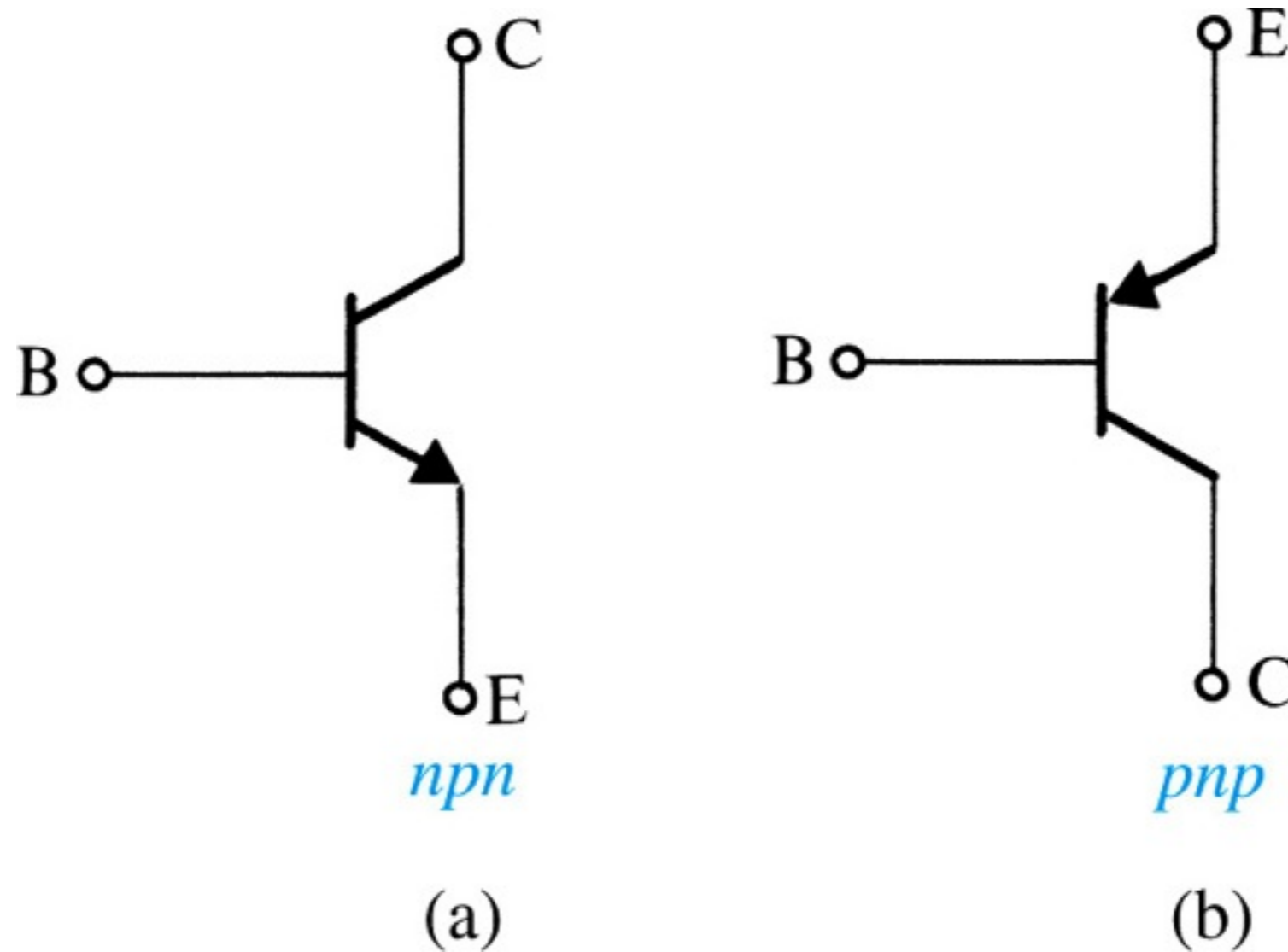


Figure 6.12: Circuit symbols for BJTs.

6.2 Two transistors, fabricated with the same technology but having different junction areas, when operated at a base-emitter voltage of 0.75 V, have collector currents of 0.2 mA and 5 mA. Find I_S for each device. What are the relative junction areas?

6.3 In a particular technology, a small BJT operating at $v_{BE} = 28V_T$ conducts a collector current of $100\ \mu\text{A}$. What is the corresponding saturation current? For a transistor in the same technology but with an emitter junction that is 32 times larger, what is the saturation current? What current will this transistor conduct at $v_{BE} = 28V_T$? What is the base–emitter voltage of the latter transistor at $i_C = 1\ \text{mA}$? Assume active-mode operation in all cases.

6.7 Consider an *npn* transistor whose base–emitter drop is 0.76 V at a collector current of 10 mA. What current will it conduct at $v_{BE} = 0.70$ V? What is its base–emitter voltage for $i_C = 10 \mu\text{A}$?

Table 6.2 Summary of the BJT Current–Voltage Relationships in the Active Mode

$$i_C = I_S e^{v_{BE}/V_T}$$

$$i_B = \frac{i_C}{\beta} = \left(\frac{I_S}{\beta}\right) e^{v_{BE}/V_T}$$

$$i_E = \frac{i_C}{\alpha} = \left(\frac{I_S}{\alpha}\right) e^{v_{BE}/V_T}$$

Note: For the *pnp* transistor, replace v_{BE} with v_{EB} .

$$i_C = \alpha i_E \qquad i_B = (1 - \alpha) i_E = \frac{i_E}{\beta + 1}$$

$$i_C = \beta i_B \qquad i_E = (\beta + 1) i_B$$

$$\beta = \frac{\alpha}{1 - \alpha} \qquad \alpha = \frac{\beta}{\beta + 1}$$

$$V_T = \text{thermal voltage} = \frac{kT}{q} \approx 25 \text{ mV at room temperature}$$

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Example 6.2

The transistor in the circuit of Fig. 6.14(a) has $\beta = 100$ and exhibits a v_{BE} of 0.7 V at $i_C = 1$ mA. Design the circuit so that a current of 2 mA flows through the collector and a voltage of +5 V appears at the collector.

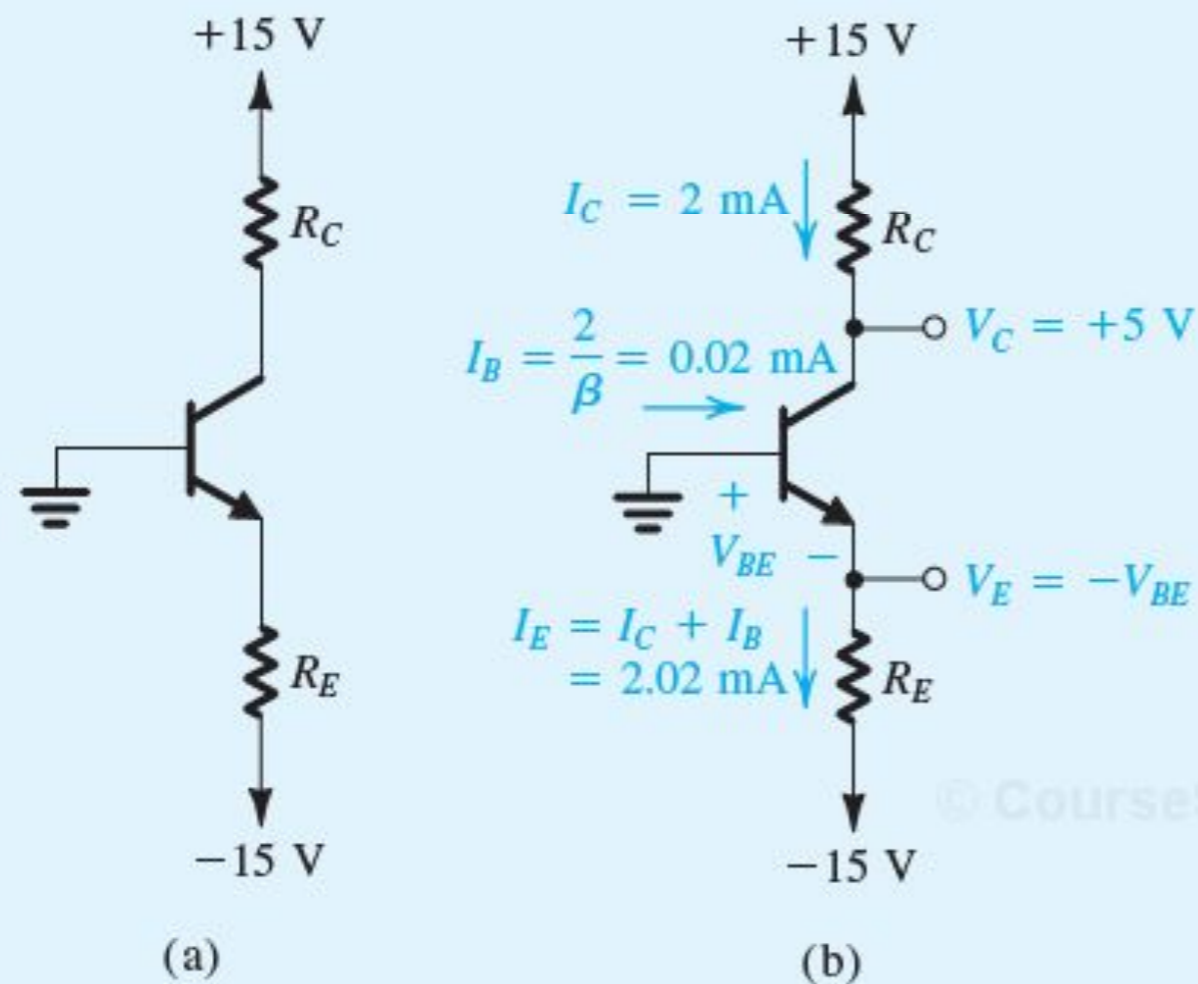


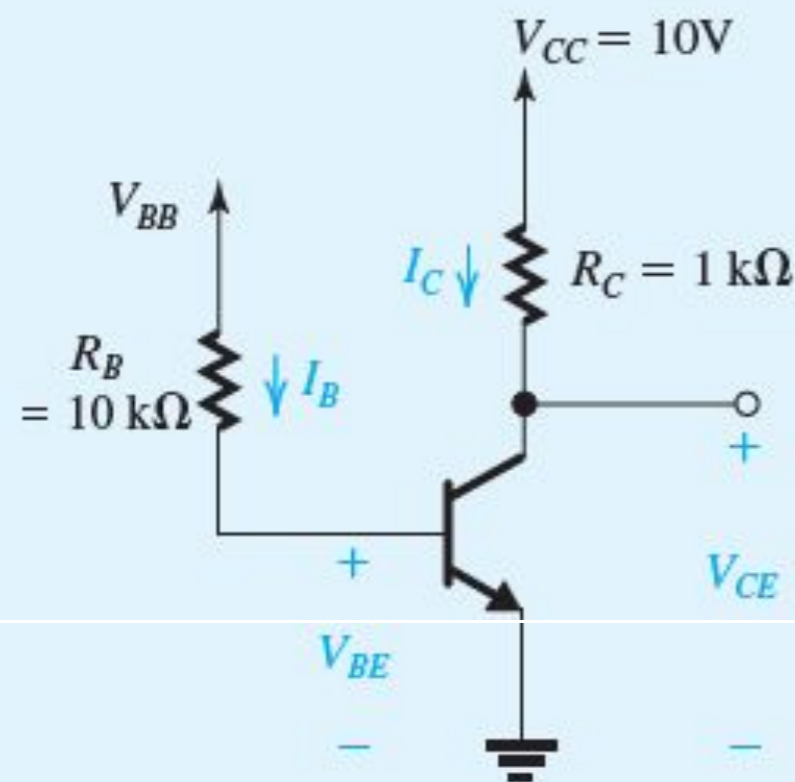
Figure 6.14 Circuit for Example 6.2.

For the circuit in Fig. 6.21, it is required to determine the value of the voltage V_{BB} that results in the transistor operating

(a) in the active mode with $V_{CE} = 5 \text{ V}$

(b) at the edge of saturation

(c) deep in saturation with $\beta_{\text{forced}} = 10$

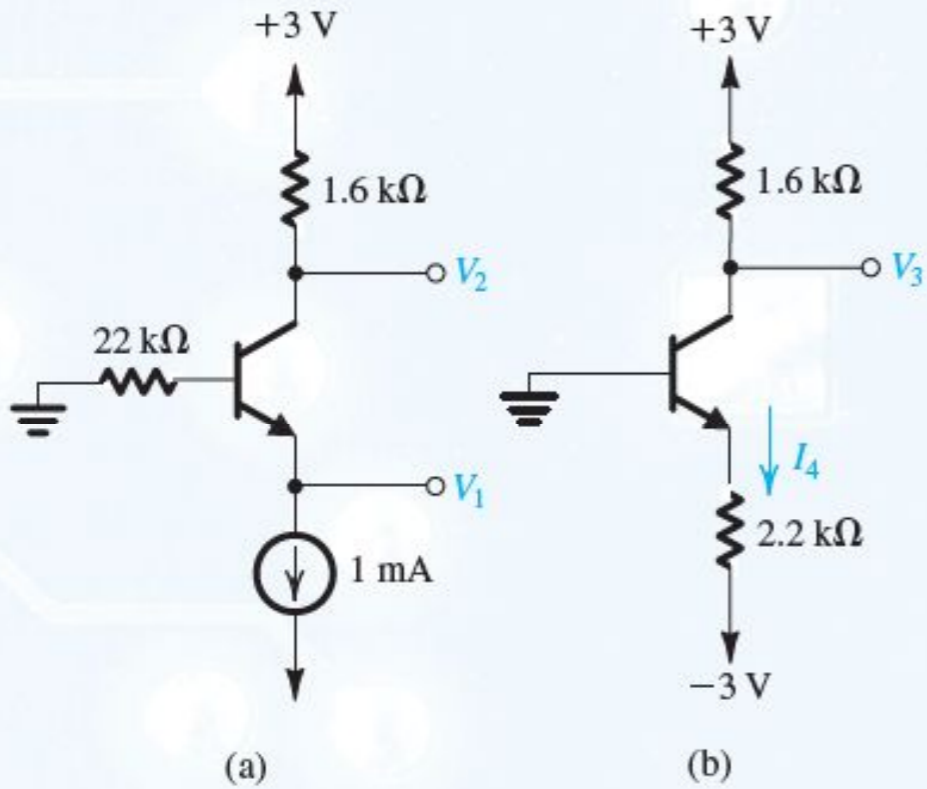


$$V_{BE} = 0.7\text{V}$$

$$\beta = 50$$

Edge of saturation: $V_{CE} = 0.3\text{V}$

Deep in saturation: $V_{CE} = 0.2\text{V}$



6.62 For the circuits in Fig. P6.62, find values for the labeled node voltages and branch currents. Assume β to be very high.

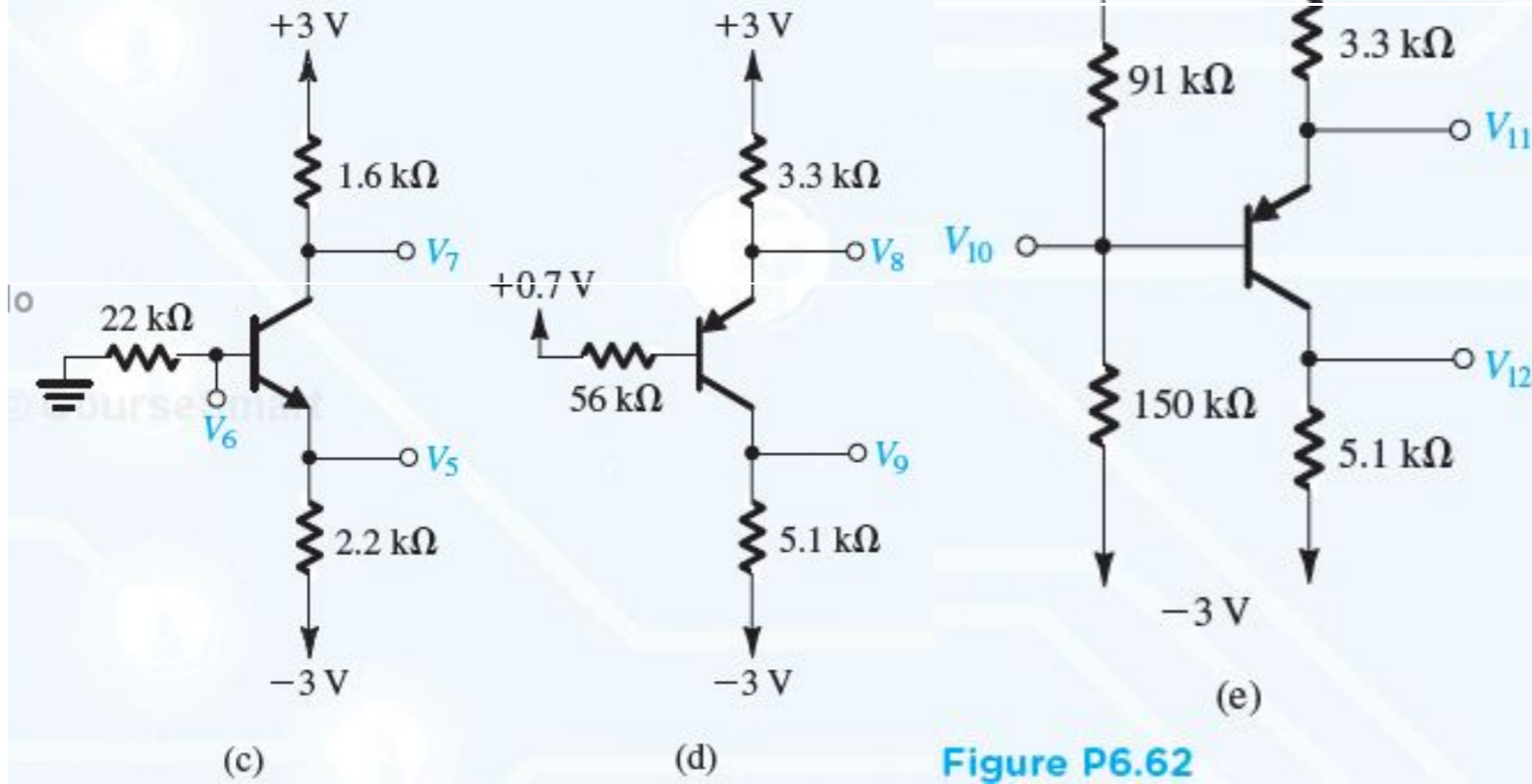


Figure P6.62