

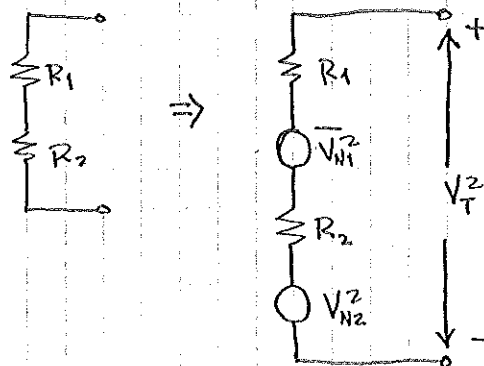
Circuit Noise Calculations

Given a noise source with PSD $\overline{I_n^2} = S_x(f) \Delta f$

The RMS value of the noise would be $I_{RMS} = \sqrt{S_x(f) \Delta f}$

- Noise source in BW Δf can be approximated by a sinusoidal generator of value i_{RMS}
- Analysis can be therefore carried using conventional circuit techniques for sinusoidal sources
- When sources are considered independent (in most cases they are) superposition can be applied

Ex: Two series resistors R_1, R_2



$V_T = V_1 + V_2$

$\Rightarrow \overline{V_T^2} = \overline{V_{N1}^2 + V_{N2}^2}$
 $= \overline{V_{N1}^2} + \overline{V_{N2}^2} + \overline{2V_{N1}V_{N2}}$

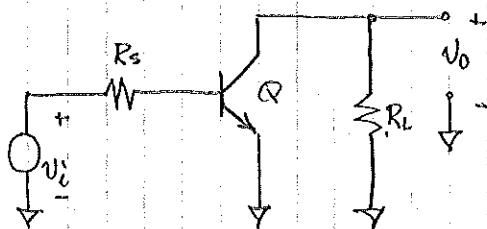
Zero for uncorrelated sources

$\overline{V_T^2} = \overline{V_{N1}^2} + \overline{V_{N2}^2}$

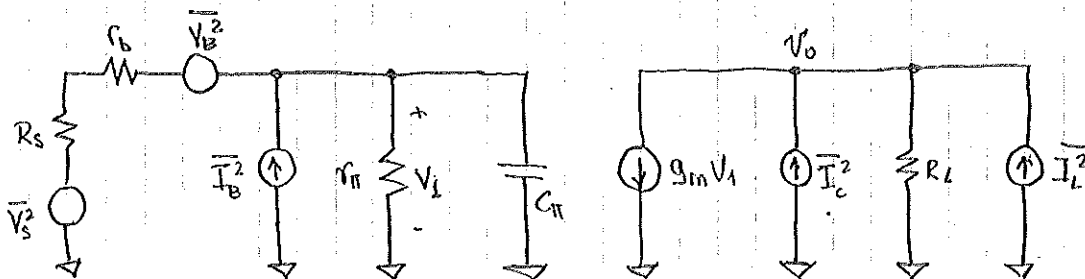
$\overline{V_{TN}^2} = 4KT R_1 + 4KT R_2$

$\Rightarrow \overline{V_{TN}^2} = 4KT (R_1 + R_2)$

Performance of a CE circuit:



- Input sources are shorted ($v_i = 0$)
- C_{μ} & r_o are neglected
- Sources considered independent



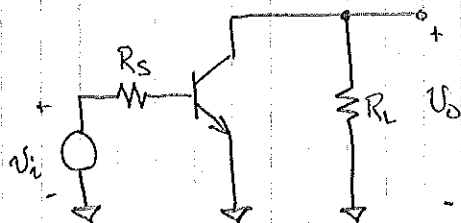
Circuit Analysis w/noise generators:

Given a noise source with PSD $\overline{I_N^2} = S_x(f)$, ← Mean sq. value of I_N

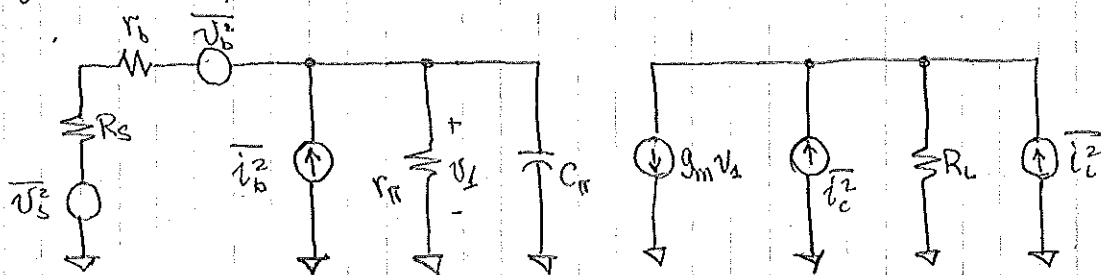
$I_N = \sqrt{S_x(f)}$ ← RMS value of I_N

- Circuit analysis can be performed by replacing I_N by a sinusoidal generator and performing sinusoidal circuit analysis.
- In most cases, multiple noise sources are uncorrelated, making it possible to apply superposition.

Example: CE Amplifier circuit



The small signal equivalent circuit with noise sources (neglects v_i , C_{μ} , and r_o)



Noise sources

$\overline{v_s^2} = 4kTR_s$ ← Thermal noise in R_s

$\overline{v_b^2} = 4kTR_b$ ← " " " " r_b

$\overline{i_b^2} = 2qI_b + k_1 \frac{I_b^2}{f} + k_2 \frac{I_b^2}{f + (1/4c)^2}$ ← Shot + Flicker + Burst
neglect

$\overline{i_c^2} = 2qI_c$ ← Shot

$\overline{v_e^2} = 4kT \frac{1}{R_L}$ ← Thermal in R_L

The total output noise can be found by superposition

22-141 50 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS



$$\overline{V_b^2} = 4KTR_b$$

$$\overline{I_L^2} = 4KT \frac{1}{R_L}$$

Applyn superposition

• Effect of $\overline{V_s^2}$

$$V_1 = \frac{Z}{Z + r_b + R_s} V_s$$

$$Z = r_{\pi} \parallel \frac{1}{sC} \quad s = j\omega$$

$$Z = \frac{r_{\pi} \cdot \frac{1}{sC}}{r_{\pi} + \frac{1}{sC}}$$

$$Z = \frac{r_{\pi}}{1 + s r_{\pi} C}$$

$$V_1 = \frac{\frac{r_{\pi}}{1 + s r_{\pi} C}}{\frac{r_{\pi}}{1 + s r_{\pi} C} + r_b + R_s} V_s$$

$$V_1 = \frac{r_{\pi}}{r_{\pi} + (r_b + R_s)(1 + s r_{\pi} C)} V_s$$

$$V_{o1} = -g_m R_L V_1 = \frac{-g_m R_L r_{\pi}}{r_{\pi} + (r_b + R_s)(1 + s r_{\pi} C)}$$

$$V_{o1} = -g_m R_L \frac{Z}{Z + r_b + R_s} V_s$$

$$\overline{V_{o1}^2} = g_m^2 R_L^2 \frac{|Z|^2}{|Z + r_b + R_s|^2} \overline{V_s^2} \quad \leftarrow \text{Effect of } \overline{V_s^2}$$

$$\overline{V_{o2}^2} = g_m^2 R_L^2 \frac{|Z|^2}{|Z + r_b + R_s|^2} \overline{V_b^2} \quad \leftarrow \text{Effect of } \overline{V_b^2}$$

$$\overline{V_{o3}^2} = g_m^2 R_L^2 \frac{(R_s + r_b)^2 |Z|^2}{|Z + r_b + R_s|^2} \overline{I_b^2} \quad \leftarrow \text{Effect of } \overline{I_b^2}$$

The contribution of $\overline{I_L^2}$ and $\overline{I_C^2}$

$$\overline{V_{o4}^2} = \overline{I_L^2} R_L^2$$

$$\overline{V_{o5}^2} = \overline{I_C^2} R_L^2$$

Applyn superposition

$$\overline{V_o^2} = \sum_{n=1}^5 \overline{V_{on}^2} \quad \leftarrow \text{By independence}$$

$$\overline{V_o^2} = g_m^2 R_L^2 \frac{|Z|^2}{|Z+r_b+R_s|^2} (\overline{V_s^2} + \overline{V_B^2} + (R_s+r_b)^2 \overline{i_b^2}) + R_L^2 (\overline{I_L^2} + \overline{I_C^2})$$

Replacing the shot noise sources (neglecting flicker)

$$\overline{V_o^2} = g_m^2 R_L^2 \frac{|Z|^2}{|Z+r_b+R_s|^2} [4KT(R_s+r_b) + (R_s+r_b)^2 2qI_B] + R_L^2 [4KT \frac{1}{R_L} + 2qI_C]$$

Replacing $Z = r_{\pi} \parallel \frac{1}{j2\pi f C}$

$$\overline{V_o^2} = g_m^2 R_L^2 \frac{r_{\pi}^2}{(r_{\pi}+R_s+r_b)^2} \cdot \frac{1}{1+(f/f_1)^2} [4KT(R_s+r_b) + (R_s+r_b)^2 2qI_B]$$

$$+ R_L^2 (4KT \frac{1}{R_L} + 2qI_C), \text{ where } f_1 = \frac{1}{2\pi [r_{\pi} \parallel (R_s+r_b)] C_{\pi}}$$

Two terms:

- ① Frequency dependent part: Gain begins to fall for $f > f_1$
Therefore noise due to $\overline{V_s^2}$, $\overline{V_B^2}$, and $\overline{I_B^2}$ decays for high frequencies
- ② Constant term due to sources $\overline{I_L^2}$ and $\overline{I_C^2}$
- Actually these decay when C_{μ} not neglected

Assigning values:

$I_C = 100 \mu A$
 $R_s = 500 \Omega$
 $R_L = 5 K \Omega$

$\beta = 100$
 $C_{\pi} = 10 pF$
 $r_b = 200 \Omega$

$$\overline{V_o^2} = \frac{4.13 \times 10^{-15}}{1+(f/f_1)^2} + 0.88 \times 10^{-15} V^2/Hz$$

$$r_{\pi} = \frac{\beta}{g_m}$$

$f_1 = 23.3 MHz$

$r_{\pi} = \frac{\beta}{g_m}$ $g_m = \frac{I_C}{\Phi_T}$ $\Phi_T = \frac{KT}{q} = 26mV @ 300^{\circ}K$

In a 0-1MHz b.w there is no decay
 $\Rightarrow \overline{V_n^2}$ constant at $5 \times 10^{-15} V^2/Hz$

$$\begin{aligned} \overline{V_o^2} &= \int_0^{1MHz} \overline{V_n^2} df \\ &= 5 \times 10^{-15} \times 10^6 \\ &= 5 \times 10^{-9} V^2 \end{aligned}$$

$V_{o,T} = \sqrt{\overline{V_o^2}} = 71 \mu V$
RMS

