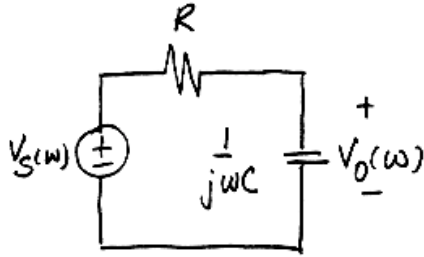


Chapter 13: Frequency Response

Ex. 13.3-1



$$H(\omega) = \frac{V_o(\omega)}{V_s(\omega)} = \frac{1}{1 + j\omega CR}$$

$$\text{gain} = \frac{1}{\sqrt{1 + (\omega CR)^2}}$$

$$\text{phase shift} = -\tan^{-1} \omega CR$$

When $R = 10^4$, $\omega = 100$, and $C = 10^{-6}$, then

$$\text{gain} = \frac{1}{\sqrt{2}} = 0.707, \text{ phase shift} = -45^\circ$$

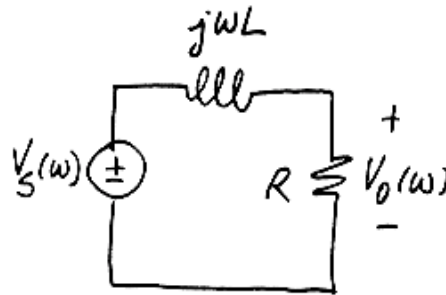
Ex. 13.3-2

$$H(\omega) = \frac{V_o(\omega)}{V_s(\omega)} = \frac{R}{R + j\omega L}$$

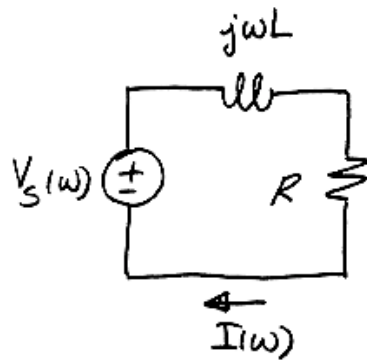
$$\text{gain} = \frac{R}{\sqrt{R^2 + (\omega L)^2}}$$

$$0.6 = \frac{30}{\sqrt{30^2 + (2\omega)^2}}$$

$$\omega = \frac{\sqrt{\left(\frac{30}{.6}\right)^2 - 30^2}}{2} = 20 \text{ rad/s}$$



Ex. 13.3-3



$$H(\omega) = \frac{I(\omega)}{V_s(\omega)} = \frac{1}{R + j\omega L}$$

$$\text{gain} = \frac{1}{\sqrt{R^2 + (\omega L)^2}}$$

$$\text{phase shift} = -\tan^{-1} \frac{\omega L}{R}$$

When $R = 30$, $L = 2$, and $\omega = 20$, then

$$\text{gain} = \frac{1}{\sqrt{30^2 + 40^2}} = 0.02 \frac{\text{A}}{\text{V}}$$

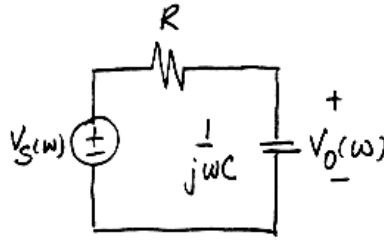
$$\text{phase shift} = -\tan^{-1} \left(\frac{40}{30} \right) = -53.1^\circ$$

Ex. 13.3-4

$$H(\omega) = \frac{V_o(\omega)}{V_s(\omega)} = \frac{1}{1 + j\omega CR}$$

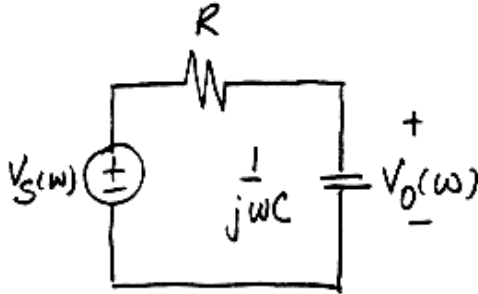
$$\text{gain} = \frac{1}{\sqrt{1 + (\omega CR)^2}}$$

$$\text{phase shift} = -\tan^{-1}\omega CR$$



$$-45^\circ = -\tan^{-1}(20 \cdot 10^{-6} \cdot R) \Rightarrow R = \frac{\tan(45^\circ)}{20 \cdot 10^{-6}} = 50 \cdot 10^3 \Omega$$

Ex. 13.3-5



$$H(\omega) = \frac{V_o(\omega)}{V_s(\omega)} = \frac{1}{1 + j\omega CR}$$

$$\text{gain} = \frac{1}{\sqrt{1 + (\omega CR)^2}}$$

$\omega, C,$ and R are all positive, or at least nonnegative, so $\text{gain} \leq 1$. These specifications cannot be met.

Ex. 13.4-1

(a) $\text{dB} = 20 \log(.5) = \underline{-6.02 \text{ dB}}$

(b) $\text{dB} = 20 \log 2 = \underline{6.02 \text{ dB}}$

Ex. 13.4-2

$$20 \log H = 20 \log \left(\frac{1}{\omega^2} \right) = 20 \log (\omega)^{-2} = -40 \log \omega$$

$$\text{slope} = 20 \log H(\omega_2) - 20 \log H(\omega_1) = -40 \log \omega_2 + 40 \log \omega_1 = -40 \log \left(\frac{\omega_2}{\omega_1} \right)$$

let $\omega_2 = 10 \omega_1$ to consider 1 decade, then

$$\text{slope} = \underline{-40 \log 10 = -40 \text{ dB/decade}}$$

Ex. 13.4-3

When $\omega C \gg B$, $H(\omega) \approx \frac{j\omega A}{j\omega C} = \frac{A}{C}$

(d) $|H(\omega)|, \text{ dB} = 20 \log_{10} |H(\omega)| = \underline{20 \log_{10} \left(\frac{A}{C} \right)}$

(b) $|H(\omega)|$ does not depend on ω so slope = 0

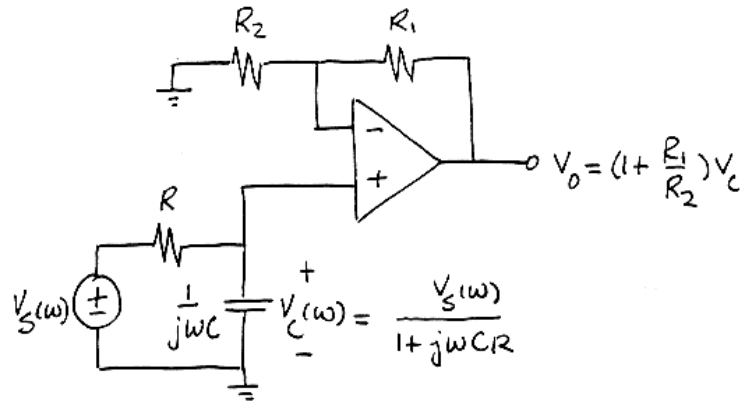
When $\omega C \ll B$, $H(\omega) \approx \frac{j\omega A}{B} = j\omega \left(\frac{A}{B} \right)$

$$|H(\omega)|, \text{ dB} = 20 \log_{10} |H(\omega)| = 20 \log_{10} \omega + 20 \log_{10} \left(\frac{A}{B} \right)$$

(c) The slope is the coefficient of $20 \log_{10} \omega$, that is, slope = 20 dB/decade

(a) The break frequency is the frequency at which $\omega C = B$, that is, $\omega = \frac{B}{C}$

Ex. 13.4-4

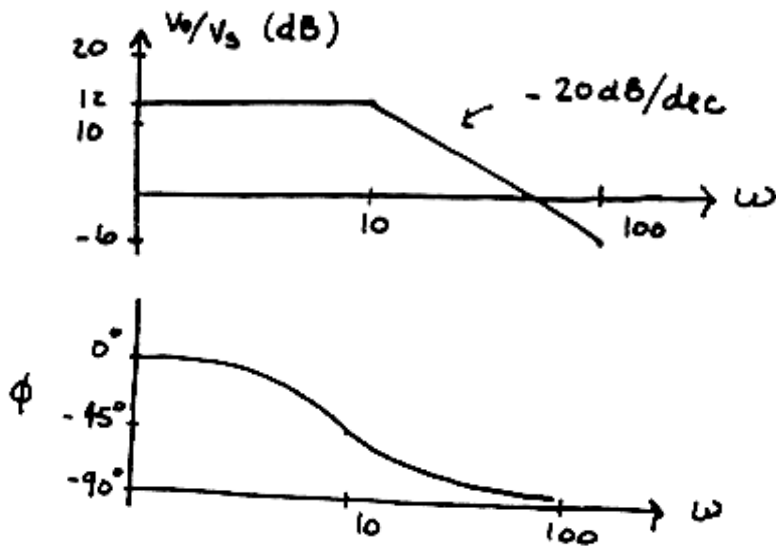


$$V_o(\omega) = \left(1 + \frac{R_1}{R_2}\right) V_c(\omega) = \left(1 + \frac{R_1}{R_2}\right) \frac{1}{1 + j\omega CR} V_s(\omega)$$

$$H(\omega) = \frac{V_o(\omega)}{V_s(\omega)} = \left(1 + \frac{R_1}{R_2}\right) \frac{1}{1 + j\omega CR}$$

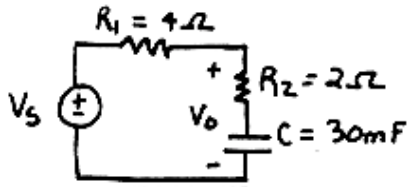
When $RC = 0.1$ and $\frac{R_1}{R_2} = 3$, then

$$H(\omega) = \frac{4}{1 + j\frac{\omega}{10}}$$



Ex. 13.4-5

a)

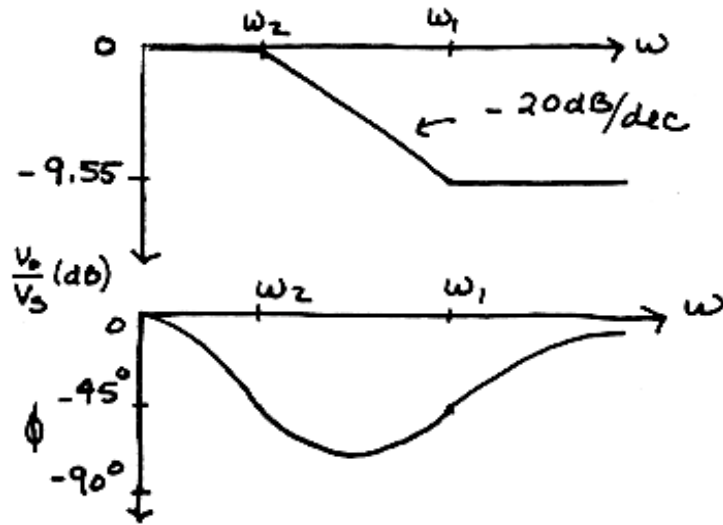


$$Z_o = R_2 + 1/j\omega C$$

$$\frac{V_o}{V_s} = \frac{Z_o}{R_1 + Z_o} = \frac{R_2 + \frac{1}{j\omega C}}{R_1 + R_2 + \frac{1}{j\omega C}} = \frac{1 + j\omega/\omega_1}{1 + j\omega/\omega_2}$$

where $\omega_1 = 1/R_2 C = 16.7 \text{ rad/s}$

$$\omega_2 = \frac{1}{(R_1 + R_2)C} = 5.56 \text{ rad/s}$$

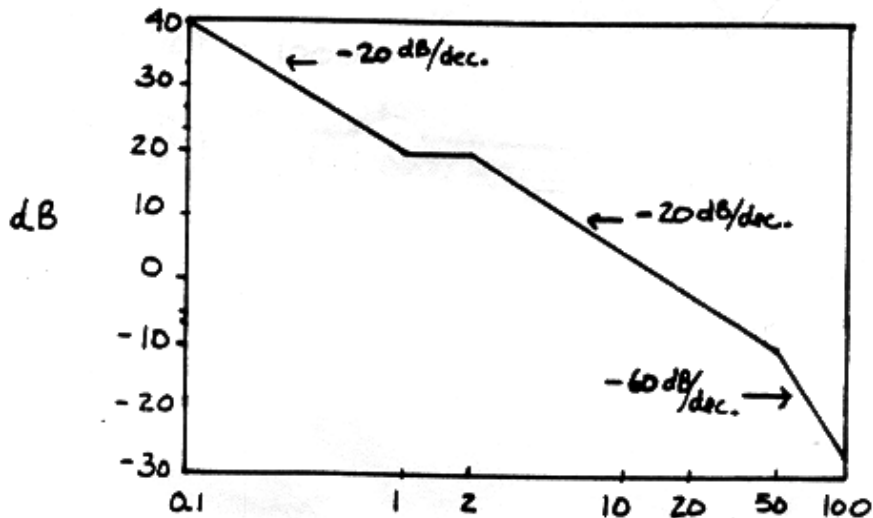


$$v_s = 10 \cos 20t \text{ or } V_s = 10 \angle 0^\circ$$

$$\therefore \frac{V_o}{V_s} = \frac{1 + j\left(\frac{20}{16.7}\right)}{1 + j\left(\frac{20}{5.56}\right)} = \frac{1 + j 1.20}{1 + j 3.60} = 0.417 \angle -24.3^\circ$$

b) So $v_o = 4.17 \angle -24.3^\circ \Rightarrow \underline{v_o(t) = 4.17 \cos(20t - 24.30) \text{ V}}$

Ex. 13.4-6



Ex. 13.5-1

$$(a) \quad Q = \omega_o RC = R\sqrt{\frac{C}{L}} = 8000\sqrt{\frac{2.5 \times 10^{-7}}{40 \times 10^{-3}}} = \underline{20}$$

$$(b) \quad BW = \frac{\omega_o}{Q} = \frac{1}{Q\sqrt{LC}} = \frac{1}{20\sqrt{(40 \times 10^{-3})(2.5 \times 10^{-7})}} = \underline{500 \text{ rad/s}}$$

Ex. 13.5-2

$$Q = \omega_o/BW = 10^7/2 \times 10^5 = \underline{50}$$

$$\text{Now } \omega_o = \frac{1}{\sqrt{LC}} \Rightarrow L = \frac{1}{\omega_o^2 C} = \frac{1}{(10^7)^2 (10 \times 10^{-12})} = \underline{1 \text{ mH}}$$

Ex. 13.5-3

$$\omega_o = \frac{1}{\sqrt{LC}} = \frac{1}{[(10^{-3})(10^{-5})]^{1/2}} = 10^4 \text{ rad/s}$$

$$Q = \omega_o/BW = 10^4/2\pi(15.9) = \underline{100}$$

$$R = \frac{\omega_o L}{Q} = \frac{(10^4)(10^{-3})}{100} = \underline{0.1\Omega}$$

Ex. 13.5-4

$$(a) \quad \omega_o = \frac{1}{\sqrt{LC}} \Rightarrow C = \frac{1}{(10^6)^2 (0.01)} = \underline{100 \text{ pF}}$$

$$Q = \omega_o/BW = 1/\omega_o RC \Rightarrow R = \frac{BW}{\omega_o^2 C} = \frac{10^3}{(10^6)^2 (10^{-10})} = \underline{10\Omega}$$

$$(b) \quad Q = \omega_o/BW = 10^6/10^3 = 1000$$

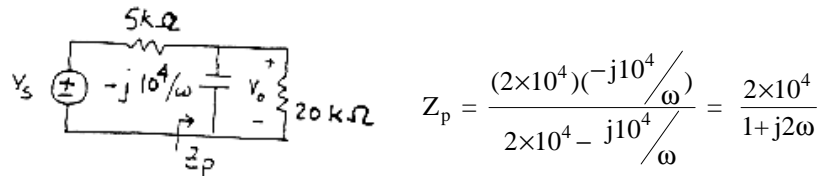
$$H = \frac{1}{1+jQ\left(\frac{\omega}{\omega_o} - \frac{\omega_o}{\omega}\right)} = \frac{1}{1+j1000\left[\frac{1.05 \times 10^6}{10^6} - \frac{10^6}{1.05 \times 10^4}\right]}$$

$$H = \frac{1}{1+j97.6}$$

Problems

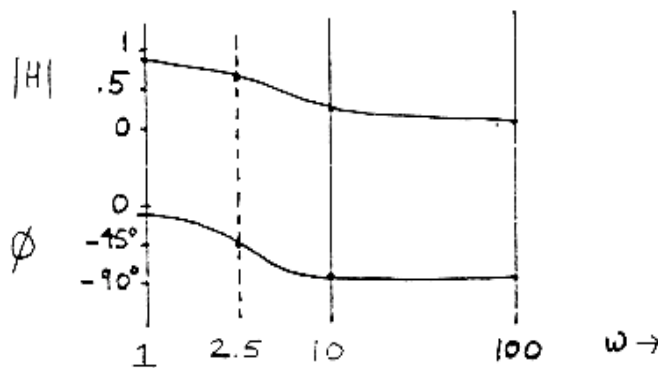
Section 13-3: Gain, Phase Shift, and the Network Function

P13.3-1



$$Z_p = \frac{(2 \times 10^4)(-j10^4/\omega)}{2 \times 10^4 - j10^4/\omega} = \frac{2 \times 10^4}{1 + j2\omega}$$

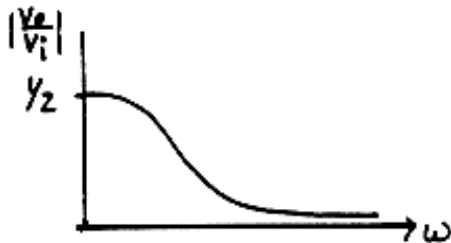
$$\therefore H(j\omega) = \frac{V_o}{V_s} = \frac{Z_p}{Z_p + 5000} = \frac{4}{[5 + j2\omega]} \Rightarrow |H(j\omega)| = \frac{4}{[(2\omega)^2 + 5^2]^{1/2}} \Rightarrow \phi(\omega) = -\tan^{-1} \frac{2\omega}{5}$$



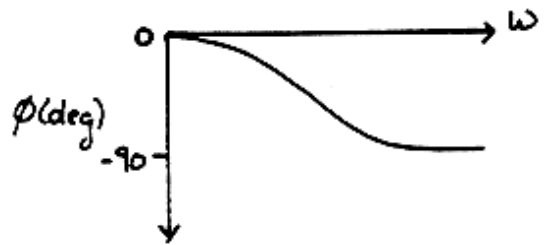
P13.3-2

$$a) \frac{V_o}{V_i} = \frac{\frac{R/sC}{R + 1/sC}}{R + \frac{R/sC}{R + 1/sC}} = \frac{1}{2 + RsC} = \frac{1}{2 + j\omega RC}$$

$$b) \Rightarrow \left| \frac{V_o}{V_i} \right| = \frac{1}{\sqrt{4 + (\omega RC)^2}}$$



(c)



Above gives correct limiting results. At $\omega = 0$, the cap is open, so dc voltage divider yields

$$\frac{V_o}{V_i} = \frac{1}{2}. \text{ At } \omega = \infty$$

$$\text{Cap is a short} \Rightarrow \frac{V_o}{V_i} = 0$$

At $\omega = 0$, V_i and V_o are in phase. At $\omega = \infty$, V_o lags

$$I_C = V_i / R \text{ by } 90^\circ$$

P13.3-3

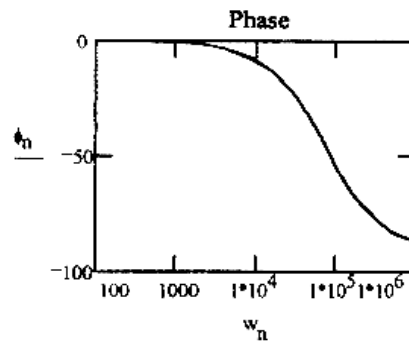
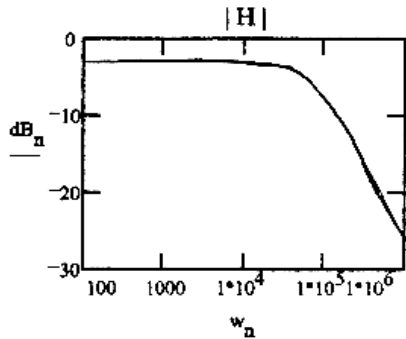
$$\frac{V_o(\omega)}{V_s(\omega)} = \frac{50}{20 + j\omega(10^{-3}) + 50} = \frac{50,000}{j\omega + 70,000}$$

MathCad Analysis

$$N := 100 \quad n := 0 .. N$$

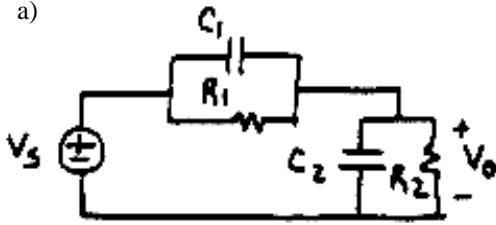
$$\omega_{\min} := 10^2 \quad \omega_{\max} := 10^6 \quad m := \ln\left(\frac{\omega_{\max}}{\omega_{\min}}\right) \quad \omega_n := \omega_{\min} \cdot e^{\frac{n}{N} \cdot m}$$

$$H_n := \frac{50000}{j \cdot \omega_n + 70000} \quad \text{dB}_n := 20 \log(|H_n|) \quad \phi_n := \arg(H_n) \cdot \frac{180}{\pi}$$



P13.3-4

a)



From voltage divider

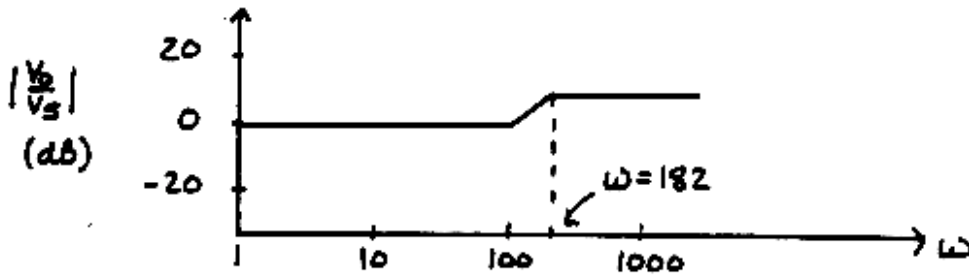
$$V_o = \frac{\frac{R_2/sC_2}{R_2 + 1/sC_2}}{\frac{R_2/sC_2}{R_2 + 1/sC_2} + \frac{R_1/sC_1}{R_1 + 1/sC_1}} V_s$$

$$\Rightarrow \frac{V_o}{V_s} = \left(\frac{R_2}{R_1 + R_2}\right) \frac{1 + R_1 C_1 s}{1 + \left(\frac{R_1 R_2}{R_1 + R_2}\right) (C_1 + C_2) s}$$

$$\therefore \frac{V_o}{V_s} = \frac{R_2}{R_1 + R_2} = K \quad \text{when } R_1 C_1 = \frac{R_1 R_2}{R_1 + R_2} (C_1 + C_2)$$

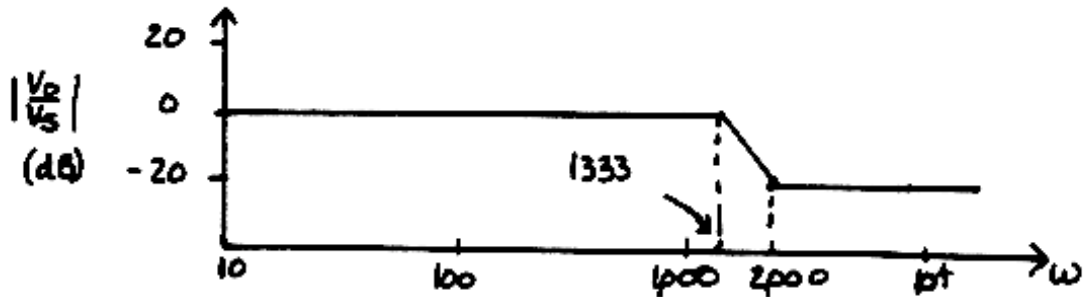
$$\Rightarrow \underline{R_1 C_1 = R_2 C_2}$$

(b) $\underline{C_1 = 1\mu\text{F}}$ $\frac{V_o}{V_s} = \frac{1}{2} \frac{1 + j\omega (10^{-2})}{1 + j\omega (5.5 \times 10^{-3})}$

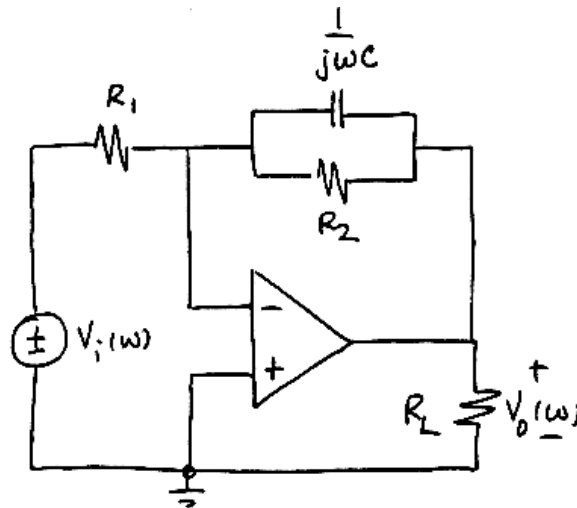


$$C_1 = 0.1 \mu\text{F}, \frac{V_o}{V_s} = \frac{1}{2} = \text{constant} \therefore 20 \log \left| \frac{V_o}{V_s} \right| = \underline{-3\text{dB (constant)}}$$

$$C_1 = 0.05 \mu\text{F}, \quad 2 \frac{V_o}{V_s} = \frac{1 + j\omega(5 \times 10^{-4})}{1 + j\omega(7.5 \times 10^{-3})}$$



P13.3-5

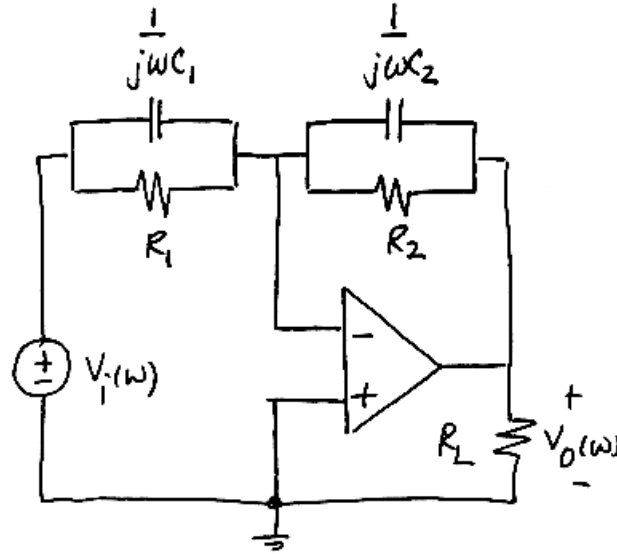


$$\begin{aligned} H(\omega) &= \frac{V_o(\omega)}{V_i(\omega)} \\ &= -\frac{R_2 \parallel \frac{1}{j\omega C}}{R_1} \\ &= \frac{-(R_2/R_1)}{1 + j\omega CR_2} \end{aligned}$$

When $R_1 = 10 \text{ k}\Omega$, $R_2 = 50 \text{ k}\Omega$, and $C = 2 \mu\text{F}$, then

$$R_2/R_1 = 5 \text{ and } R_2 C = \frac{1}{10} \text{ so } H(\omega) = \frac{-5}{1 + j\frac{\omega}{10}}$$

P13.3-6



$$\begin{aligned}
 H(\omega) &= \frac{V_o(\omega)}{V_i(\omega)} \\
 &= -\frac{R_2 \parallel \frac{1}{j\omega C_2}}{R_1 \parallel \frac{1}{j\omega C_1}} \\
 &= -\frac{R_2}{1 + j\omega C_2 R_2} \frac{1 + j\omega C_1 R_1}{R_1}
 \end{aligned}$$

$$H(\omega) = -\left(\frac{R_2}{R_1}\right) \left(\frac{1 + j\omega C_1 R_1}{1 + j\omega C_2 R_2}\right)$$

When $R_1 = 10\text{k}\Omega$, $R_2 = 50\text{k}\Omega$, $C_1 = 4\mu\text{F}$ and

$C_2 = 2\mu\text{F}$, then $\frac{R_2}{R_1} = 5$, $C_1 R_1 = \frac{1}{25}$ and $C_2 R_2 = \frac{1}{10}$

so
$$H(\omega) = -5 \left(\frac{1 + j\frac{\omega}{25}}{1 + j\frac{\omega}{10}} \right)$$

$$\text{gain} = |H(\omega)| = 5 \frac{\sqrt{1 + \frac{\omega^2}{625}}}{\sqrt{1 + \frac{\omega^2}{100}}}$$

$$\text{phase shift} = \angle H(\omega) = 180 + \tan^{-1} \frac{\omega}{25} - \tan^{-1} \frac{\omega}{10}$$

P13.3-7

$$R_3 \parallel \frac{1}{j\omega C} = \frac{R_3 \frac{1}{j\omega C}}{R_3 + \frac{1}{j\omega C}} = \frac{R_1}{1 + j\omega C R_3}$$

$$T(\omega) = -\frac{R_2 + \frac{R_3}{1 + j\omega C R_3}}{R_1} = -\frac{R_2 + R_3 + j\omega R_2 R_3 C}{R_1 + j\omega R_1 R_3 C}$$

$$5 = \lim_{\omega \rightarrow 0} |T(\omega)| = \frac{R_2 + R_3}{R_1}$$

$$2 = \lim_{\omega \rightarrow \infty} |T(\omega)| = \frac{R_2}{R_1} \Rightarrow R_2 = 2R_1 = 20\text{k}\Omega$$

then $R_3 = 5R_1 - R_2 = 30\text{k}\Omega$

P13.3-8

$$T(\omega) = -\frac{R_2 + \frac{1}{j\omega C}}{R_1} = -\frac{1 + j\omega CR_2}{j\omega CR_1}$$

$$\angle T(\omega) = 180^\circ + \tan^{-1}\omega CR_2 - 90$$

$$\angle T(\omega) = 135^\circ \Rightarrow \tan^{-1}\omega CR_2 = 45$$

$$\Rightarrow \omega CR_2 = 1$$

$$\Rightarrow R_2 = \frac{1}{10^3 10^{-7}} = 10\text{k}\Omega$$

$$10 = \lim_{\omega \rightarrow \infty} |T(\omega)| = \frac{R_2}{R_1} \Rightarrow R_1 = \frac{R_2}{10} = 1\text{k}\Omega$$

P13.3-9

$$T(\omega) = \frac{-R_2}{\frac{1}{j\omega C} + j\omega CR_1} = -\frac{j\omega CR_2}{1 + j\omega CR_1}$$

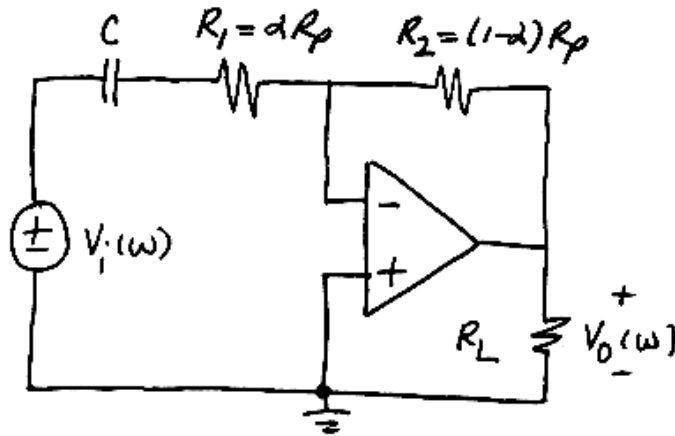
$$10 = \lim_{\omega \rightarrow \infty} |T(\omega)| = \frac{R_2}{R_1} \Rightarrow R_2 = 10R_1$$

$$\angle T(\omega) = 180 + 90 - \tan^{-1}\omega CR_1$$

$$\Rightarrow R_1 = \frac{\tan(270 - \angle T(\omega))}{\omega C} = 10^4 \cdot \tan(270 - \angle T(\omega)) = 10^4 = 10\text{k}\Omega$$

$$\Rightarrow R_2 = 100\text{k}\Omega$$

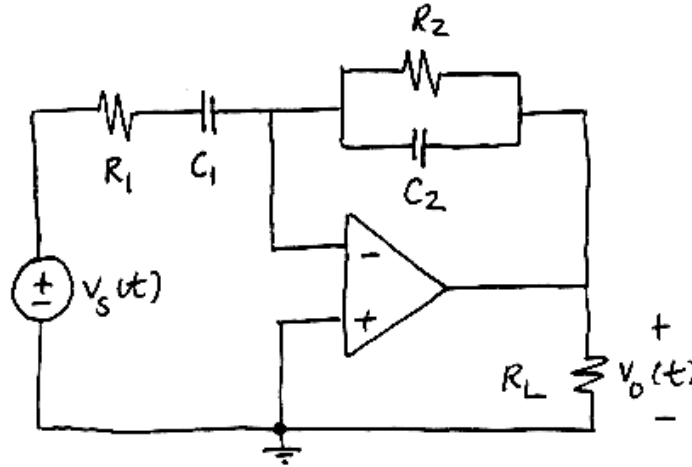
P13.3-10



$$H(\omega) = \frac{V_o(\omega)}{V_i(\omega)} = -\frac{R_2}{R_1 + \frac{1}{j\omega C}} = -\frac{j\omega CR_2}{1 + j\omega CR_1} = -\frac{j\omega C(1-\alpha)R_p}{1 + j\omega C\alpha R_p}$$

$$4 = \lim_{\omega \rightarrow \infty} |H(\omega)| = \frac{1-\alpha}{\alpha} \Rightarrow \alpha = 0.2$$

P13.3-11



$$H(\omega) = \frac{V_o(\omega)}{V_s(\omega)} = -\frac{R_2 \parallel \frac{1}{j\omega C_2}}{R_1 + \frac{1}{j\omega C_1}} = -C_1 R_2 \frac{j\omega}{(1 + j\omega R_1 C_1)(1 + j\omega R_2 C_2)}$$

When $R_1 = 5\text{k}\Omega$, $C_1 = 1\mu\text{F}$, $R_2 = 10\text{k}\Omega$ and $C_2 = 0.1\mu\text{F}$, then

$$H(\omega) = -0.01 \frac{j\omega}{\left(1 + j\frac{\omega}{200}\right)\left(1 + j\frac{\omega}{1000}\right)}$$

So

ω	$ H(\omega) $	$\angle H(\omega)$
0	0	-90°
500	1.66	175°
2500	0.74	116°

Then

$$v_o(t) = (0)50 + (1.66)30 \cos(500t + 115^\circ + 175^\circ) - (0.74)20 \cos(2500t + 30^\circ + 116^\circ) \\ = 49.8 \cos(500t - 70^\circ) - 14.8 \cos(2500t + 146^\circ) \text{ mV}$$

When $R_1 = 5\text{k}\Omega$, $C_1 = 1\mu\text{F}$, $R_2 = 10\text{k}$ and $C_2 = 0.01\mu\text{F}$, then

$$H(\omega) = -0.01 \frac{j\omega}{\left(1 + j\frac{\omega}{200}\right)\left(1 + j\frac{\omega}{10,000}\right)}$$

So

ω	$ H(\omega) $	$\angle H(\omega)$
0	0	-90°
500	1.855	-161°
2500	1.934	170°

Then

$$v_o(t) = (0)50 + (1.855)30 \cos(500t + 115^\circ - 161^\circ) - (1.934)20 \cos(2500t + 30^\circ + 170^\circ) \\ = 55.65 \cos(500t - 46^\circ) - 38.68 \cos(2500t + 190^\circ) \text{ mV}$$

P13.3-12

$$a) \quad |V_s| = \frac{(8 \text{ div}) \left(\frac{2 \text{ V}}{\text{div}} \right)}{2} = 8 \text{ V}$$

$$|V_o| = \frac{(6.2 \text{ div}) \left(\frac{2 \text{ V}}{\text{div}} \right)}{2} = 6.2 \text{ V}$$

$$\text{gain} = \frac{|V_o|}{|V_s|} = \frac{6.2}{8} = 0.775$$

$$b) \quad H(\omega) = \frac{V_o(\omega)}{V_s(\omega)} = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{1}{1 + j\omega CR}$$

$$|H(\omega)| = \frac{1}{\sqrt{1 + \omega^2 C^2 R^2}}$$

$$\text{Let } g = |H(\omega)| = \frac{1}{\sqrt{1 + \omega^2 C^2 R^2}}$$

Then

$$C = \frac{1}{\omega R} \sqrt{\left(\frac{1}{g}\right)^2 - 1}$$

In this case $\omega = 2\pi \cdot 500 = 3142 \text{ rad/s}$, $|H(\omega)| = 0.775$ and $R = 1000\Omega$ so $C = 0.26\mu\text{F}$.

$$c) \quad \angle H(\omega) = -\tan^{-1} \omega RC$$

so

$$\omega = \frac{\tan(-\angle H(\omega))}{RC}$$

Recalling that $R = 1000$ and $C = 0.26\mu\text{F}$, we calculate

ω	$ H(\omega) $	$\angle H(\omega)$
$2\pi(200)$	0.95	-18°
$2\pi(2000)$	0.26	-73°

$$\text{Next, } \angle H(\omega) = -45^\circ \text{ requires } \omega = \frac{\tan(-(-45^\circ))}{(1000)(.26 \cdot 10^{-6})} = 3846 \text{ rad/s}$$

$$\text{Similarly, } \angle H(\omega) = -135^\circ \text{ requires } \omega = \frac{\tan(-(-135^\circ))}{(1000)(.26 \cdot 10^{-6})} = -3846 \text{ rad/s}$$

A negative frequency is not acceptable. We conclude that this circuit cannot produce a phase shift equal to -135° .

$$d) \quad C = \frac{\tan(-\angle H(\omega))}{\omega R}$$

$$C = \frac{\tan(-60^\circ)}{(2\pi \cdot 500)(1000)} = 0.55 \mu\text{F}$$

$$C = \frac{\tan(-(-300^\circ))}{(2\pi \cdot 500)(1000)} = -0.55 \mu\text{F}$$

A negative value of capacitance is not acceptable and indicates that this circuit cannot be designed to produce a phase shift at -300° at a frequency of 500 Hz.

$$e) \quad C = \frac{\tan(-(-120^\circ))}{(2\pi \cdot 500)(100)} = -0.55 \mu\text{F}$$

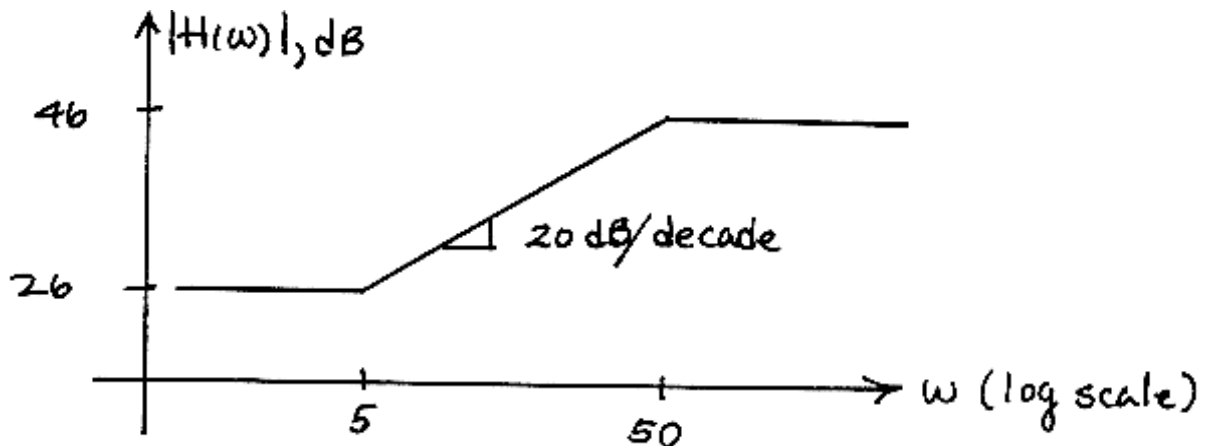
This circuit cannot be designed to produce a phase shift of -120° at 500 Hz.

Section 13-4: Bode Plots

P13.4-1

$$H(\omega) = \frac{20 \left(1 + j\frac{\omega}{5}\right)}{\left(1 + j\frac{\omega}{50}\right)}$$

$$H(\omega) \approx \begin{cases} 20 & \omega < 5 \\ 20 \left(j\frac{\omega}{5}\right) = j4\omega & 5 < \omega < 50 \\ 20 \left(\frac{j\omega}{5}\right) = 200 & 50 < \omega \end{cases}$$



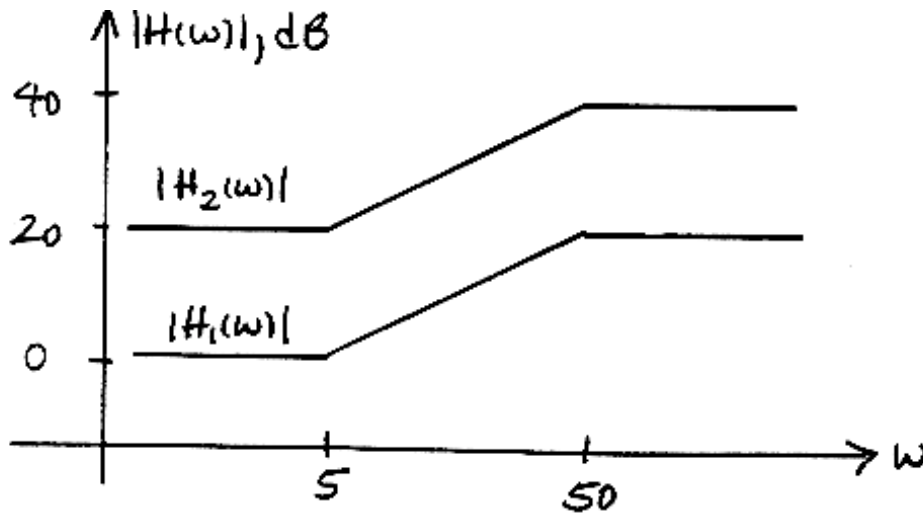
P13.4-2

$$H_1(\omega) = \frac{1 + j\frac{\omega}{5}}{1 + j\frac{\omega}{50}} \quad H_2(\omega) = 10 \frac{1 + j\frac{\omega}{5}}{1 + j\frac{\omega}{50}}$$

Both $H_1(\omega)$ and $H_2(\omega)$ have a pole at $\omega = 50\text{rad/s}$ and a zero at $\omega = 5\text{rad/s}$. The slopes of both magnitude Bode plots increase by 20dB/decade at $\omega = 5\text{rad/s}$ and decrease by 20dB/decade at $\omega = 50\text{rad/s}$. The difference is that for $\omega < 5\text{rad/s}$

and

$$\begin{aligned} |H_1(\omega)| &\approx 1 = 0 \text{ dB} \\ |H_2(\omega)| &\approx 10 = 20 \text{ dB} \end{aligned}$$



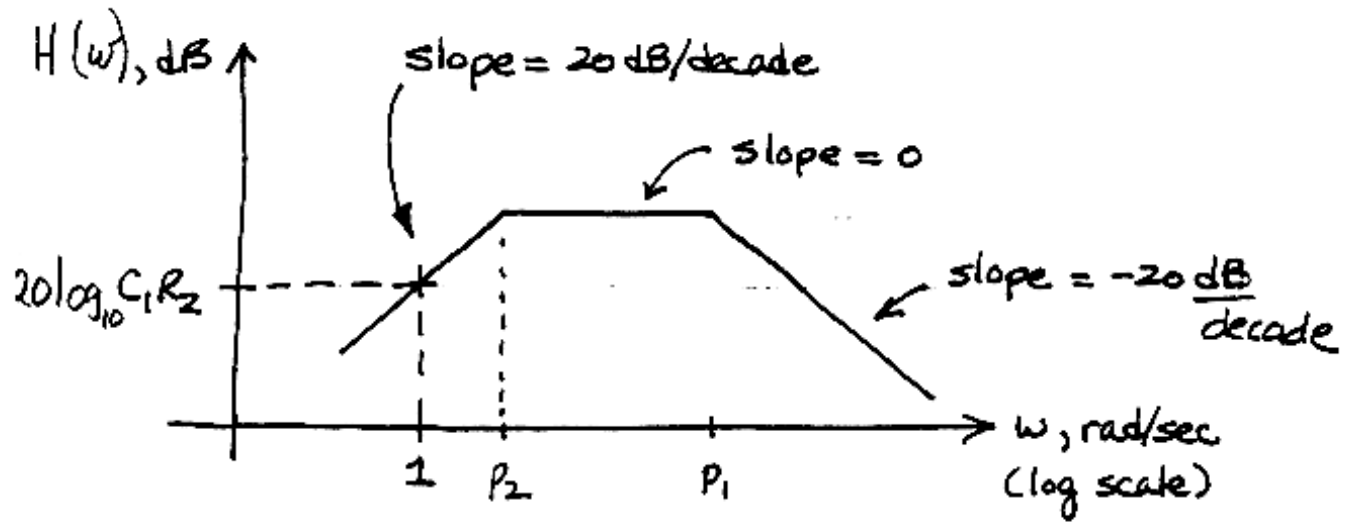
P13.4-3

$$H(\omega) = -\frac{R_2}{R_1 + \frac{1}{j\omega C_1}} = -C_1 R_2 \frac{j\omega}{(1 + j\omega R_1 C_1)(1 + j\omega R_2 C_2)}$$

This network function has poles at

$$p_1 = \frac{1}{R_1 C_1} = 2000 \text{ rad/s} \quad p_2 = \frac{1}{R_2 C_2} = 1000 \text{ rad/s}$$

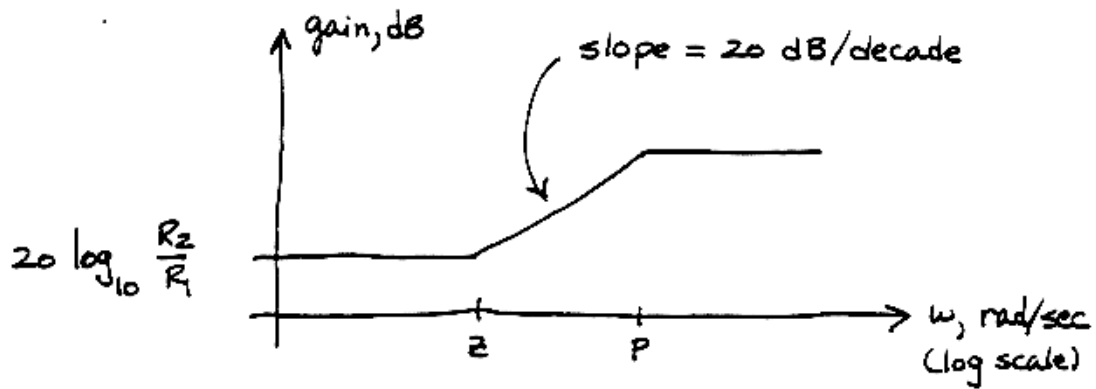
$$H(\omega) \approx \begin{cases} (C_1 R_2) j\omega & \omega < p_1 \\ (C_1 R_2) \frac{j\omega}{j\omega C_1 R_1} = \frac{R_2}{R_1} = 2 & p_1 < \omega < p_2 \\ (C_1 R_2) \frac{j\omega}{(j\omega C_1 R_1)(j\omega C_2 R_2)} = \frac{1}{j\omega C_2 R_1} & \omega > p_2 \end{cases}$$



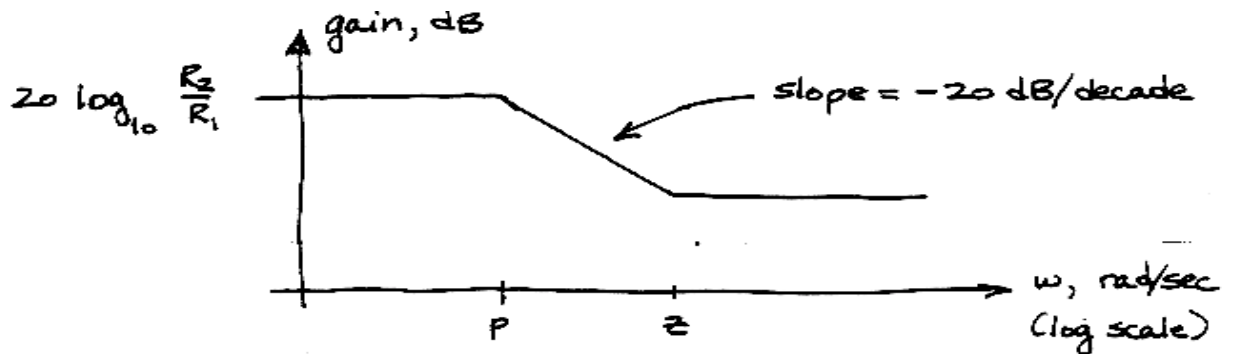
P13.4-4

$$H(\omega) = -\frac{\frac{R_2}{1+j\omega C_2 R_2}}{\frac{R_1}{1+j\omega C_1 R_1}} = -\frac{R_2(1+j\omega C_1 R_1)}{R_1(1+j\omega C_2 R_2)} \text{ so } K = -\frac{R_2}{R_1}, z = \frac{1}{C_1 R_1} \text{ and } p = \frac{1}{C_2 R_2}$$

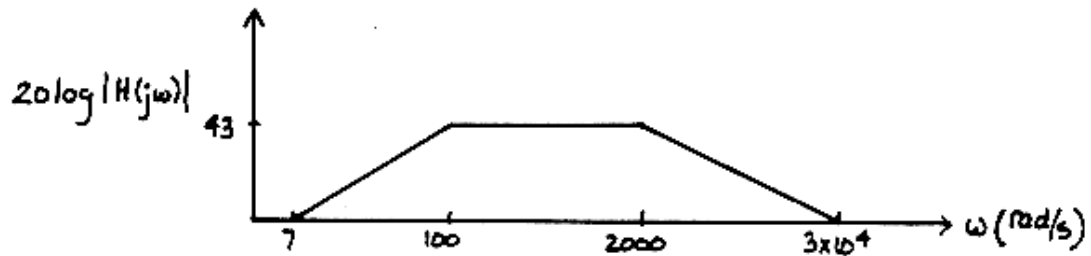
When $z < p$, then



When $p < z$, then



P13.4-5 A reasonable approximation (asymptotic) for the Bode diagram is:



$$\therefore H(j\omega) = \frac{A(1+j\omega/7)(1+j\omega/3 \times 10^4)}{(1+j/100)(1+j\omega/2000)}$$

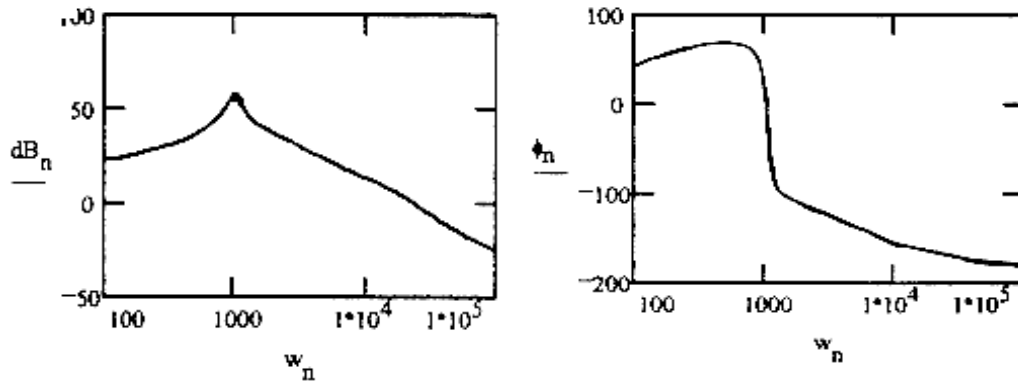
$$\text{At the peak, } H(j\omega) \approx \frac{A j\omega/7}{j\omega/100} = \frac{100}{7} A$$

$$\therefore 43 = 20 \log \left(\frac{100}{7} A \right) \Rightarrow A = 10$$

$$\Rightarrow H(j\omega) = \frac{10(1+j\omega/7)(1+j\omega/3 \times 10^4)}{(1+j/100)(1+j\omega/2000)}$$

P13.4-6

(a)



(b) $BW = \frac{\omega_0}{Q} = \frac{1000}{10} = 100$

(c) From the Bode diagram, it is clear that the overall Q of the circuit is dictated by the Q of the second order factor. Thus the overall $Q=10$

(d) From, the plot, the gain at $\omega_0 = 40\text{dB}$

P13.4-7

- The slope is 40dB/decade for low frequencies, so the numerator will include the factor $(j\omega)^2$.
- The slope decreases by 40dB/decade at $\omega = 0.7\text{rad/sec}$. So there is a second order pole at $\omega_0 = 0.7\text{rad/sec}$. The damping factor of this pole cannot be determined from the asymptotic Bode plot; call it δ_1 . The denominator of the network function will contain the factor

$$1 + 2\delta_1 j \frac{\omega}{0.7} - \left(\frac{\omega}{0.7}\right)^2$$

- The slope increases by 20dB/decade at $\omega = 10\text{rad/s}$, indicating a zero at 10rad/s.
- The slope decreases by 20dB/decade at $\omega = 100\text{rad/s}$, indicating a pole at 100rad/s.
- The slope decreases by 40dB/decade at $\omega = 600\text{rad/s}$, indicating a second order pole at $\omega_0 = 600\text{rad/s}$. The damping factor of this pole cannot be determined from an asymptotic Bode plot; call it δ_2 . The denominator of the network function will contain the factor

$$1 + 2\delta_2 j \frac{\omega}{600} - \left(\frac{\omega}{600}\right)^2$$

$$H(\omega) = \frac{K(1 + j\frac{\omega}{10})(j\omega)^2}{10 \left(1 + 2\delta_1 j \frac{\omega}{0.7} - \left(\frac{\omega}{0.7}\right)^2\right) \left(1 + 2\delta_2 j \frac{\omega}{600} - \left(\frac{\omega}{600}\right)^2\right) \left(1 + j\frac{\omega}{100}\right)}$$

To determine K, notice that $|H(\omega)|=0\text{dB}=1$ when $0.7 < \omega < 10$. That is

$$1 = \frac{K(1)(j\omega)^2}{-\left(\frac{\omega}{0.7}\right)^2 (1)(1)} = K(0.7)^2 \Rightarrow K = 2$$

P13.4-8

By inspection,

$$H(j\omega) = \frac{A(1 + j\omega/100)}{j\omega(1 + j\omega/1000)}$$

from the magnitude plot for $100 < \omega < 1000$

$$|H(j\omega)| \approx A j \frac{\omega/100}{j\omega} = A/100$$

$$\therefore 20 \log A/100 = 0 \Rightarrow A = 100$$

$$\text{So } H(j\omega) = \frac{100(1 + j\omega/100)}{j\omega(1 + j\omega/1000)}$$

P13.4-9

$$(a) \quad T(\omega) = \frac{K \left(1 + j \frac{\omega}{z}\right)}{j\omega}$$

$$|T(\omega)| = \frac{K}{\omega} \sqrt{1 + \left(\frac{\omega}{z}\right)^2}$$

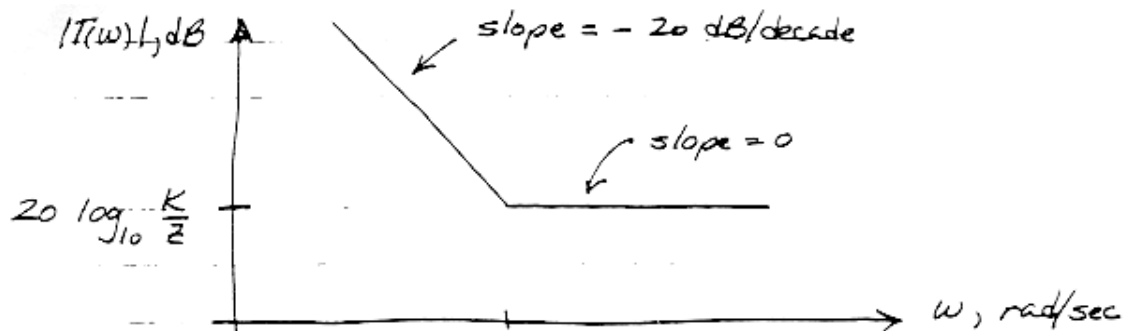
$$|T(\omega)| \text{ dB} = 20 \log_{10} \frac{K}{\omega} \sqrt{1 + \left(\frac{\omega}{z}\right)^2} = 20 \log_{10} K - 20 \log_{10} \omega + 20 \log_{10} \sqrt{1 + \left(\frac{\omega}{z}\right)^2}$$

$$\text{Let } |T_L(\omega)| \text{ dB} = 20 \log_{10} K - 20 \log_{10} \omega$$

$$\text{and } |T_H(\omega)| \text{ dB} = 20 \log_{10} \frac{K}{z}$$

$$\text{Then } |T(\omega)| \text{ dB} \approx \begin{cases} |T_L(\omega)| \text{ dB} & \omega \ll z \\ |T_H(\omega)| \text{ dB} & \omega \gg z \end{cases}$$

So $|T_L(\omega)| \text{ dB}$ and $|T_H(\omega)| \text{ dB}$ are the required low and high - frequency asymptotes.



The Bode plot will be within 1% of $|T(\omega)| \text{ dB}$ both for $\omega \ll z$ and for $\omega \gg z$. The range when $\omega \ll z$ is characterized by

$$|T_L(\omega)| = .99 |T(\omega)| \quad (\text{gains not in dB})$$

$$\Rightarrow 20 \log_{10} .99 = |T_L(\omega)| \text{ dB} - |T(\omega)| \text{ dB} \quad (\text{gains in dB})$$

$$= 20 \log_{10} K - 20 \log_{10} \omega - 20 \log_{10} \frac{K}{\omega} \sqrt{1 + \left(\frac{\omega}{z}\right)^2}$$

$$= -20 \log_{10} \sqrt{1 + \left(\frac{\omega}{z}\right)^2}$$

$$= 20 \log_{10} \frac{1}{\sqrt{1 + \left(\frac{\omega}{z}\right)^2}}$$

$$\Rightarrow .99 = \frac{1}{\sqrt{1+\left(\frac{\omega}{z}\right)^2}} \Rightarrow \omega = z\sqrt{\left(\frac{1}{.99}\right)^2 - 1} = .14z \approx \frac{z}{7}$$

The range when $\omega \gg z$ is characterized by

$$\begin{aligned} |T_H(\omega)| &= .99|T(\omega)| && \text{(gains not in dB)} \\ \Rightarrow 20 \log_{10}.99 &= |T_H(\omega)| \text{ dB} - |T(\omega)| \text{ dB} && \text{(gains in dB)} \\ &= 20 \log_{10}K - 20 \log_{10}z - 20 \log_{10} \frac{K}{\omega} \sqrt{1+\left(\frac{\omega}{z}\right)^2} \\ &= -20 \log_{10} \frac{z}{\omega} \sqrt{1+\left(\frac{\omega}{z}\right)^2} \\ &= 20 \log_{10} \frac{1}{\sqrt{\left(\frac{z}{\omega}\right)^2 + 1}} \end{aligned}$$

$$\begin{aligned} \Rightarrow \frac{z}{\omega} &= \sqrt{\left(\frac{1}{.99}\right)^2 - 1} \\ \Rightarrow \omega &= \frac{z}{\sqrt{\left(\frac{1}{.99}\right)^2 - 1}} = \frac{z}{.14} \approx 7z \end{aligned}$$

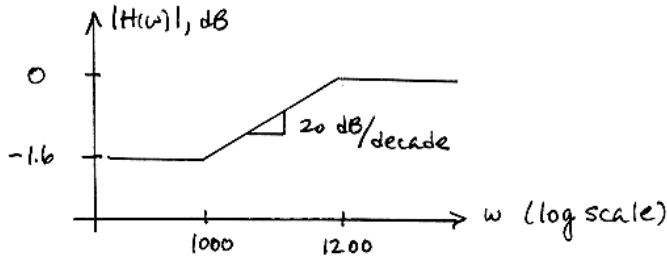
The error is less than 1% when $\omega < \frac{z}{7}$ and when $\omega > 7z$.

P13.4-10

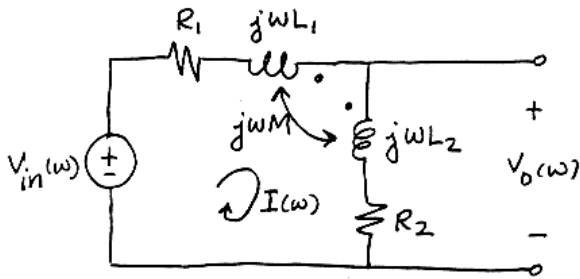
$$\begin{aligned} H(\omega) &= \frac{V_0(\omega)}{V_s(\omega)} = \frac{R_t}{R_t + R_1} \parallel \frac{1}{j\omega C} = \frac{R_t}{R_t + \frac{R_1}{1+j\omega CR_1}} \\ H(\omega) &= \frac{R_t(1+j\omega CR_1)}{R_1 + R_t + j\omega CR_1 R_t} = \left(\frac{R_t}{R_1 + R_t} \right) \frac{1+j\omega CR_1}{1+j\omega \left(\frac{CR_1 R_t}{R_1 + R_t} \right)} \end{aligned}$$

When $R_1 = 1k\Omega$, $C = 1\mu F$ and $R_t = 5k\Omega$

$$H(\omega) = \frac{5}{6} \left(\frac{1+j\frac{\omega}{1000}}{1+j\frac{\omega}{1200}} \right) \Rightarrow H(\omega) \cong \begin{cases} \frac{5}{6} & \omega < 1000 \\ \left(\frac{5}{6}\right)j\frac{\omega}{1000} & 1000 < \omega < 1200 \\ 1 & \omega > 1200 \end{cases}$$



P13.4-11



$$V_{in}(\omega) = I(\omega) [R_1 + (j\omega L_1 - j\omega M) + (-j\omega M + j\omega L_2) + R_2]$$

$$V_0(\omega) = I(\omega) [(-j\omega M + j\omega L_2) + R_2]$$

$$T(\omega) = \frac{V_0(\omega)}{V_{in}(\omega)} = \frac{R_2 + j\omega(L_2 - M)}{R_1 + R_2 + j\omega(L_1 + L_2 - 2M)}$$

$$K_1 = \lim_{\omega \rightarrow \infty} |T(\omega)| = \frac{L_2 - M}{L_1 + L_2 - 2M} = 0.75$$

$$K_2 = \lim_{\omega \rightarrow 0} |T(\omega)| = \frac{R_2}{R_1 + R_2} = 0.2$$

$$z = \frac{R_2}{L_2 - M} = 333 \text{ rad/s}$$

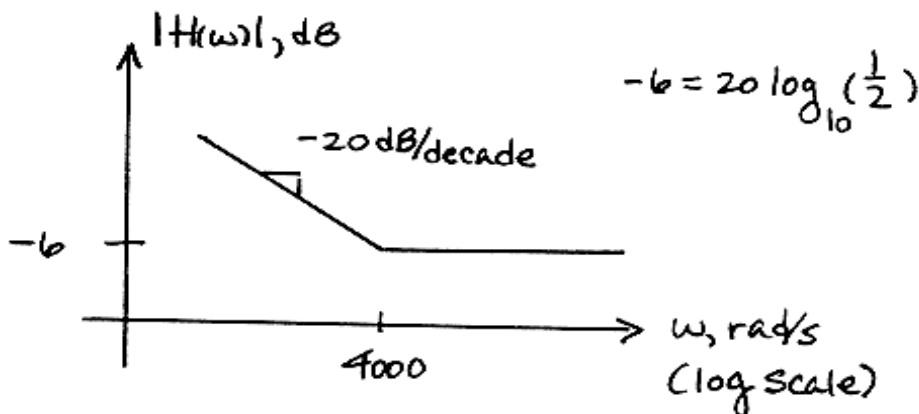
$$p = \frac{R_1 + R_2}{L_1 + L_2 - 2M} = 1250 \text{ rad/s}$$

P13.4-12

$$H(\omega) = -\frac{1}{j\omega C_2} \parallel \frac{1}{j\omega C_1} = -\frac{1 + j\omega R_1 C_1}{j\omega R_1 C_2} = -\frac{1}{R_1 C_2} \frac{(1 + j\omega R_1 C_1)}{j\omega}$$

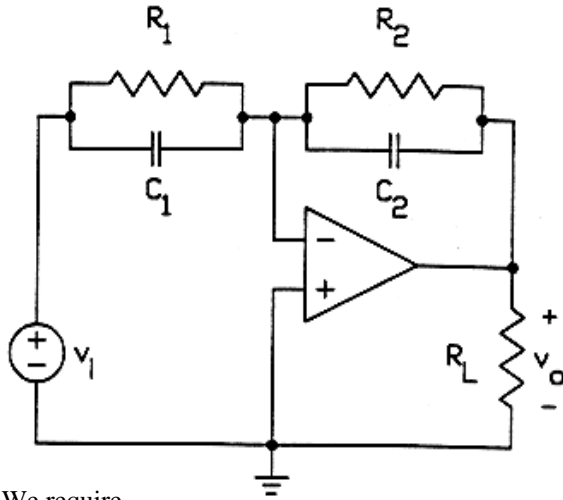
$$H(\omega) = \begin{cases} -\frac{1}{R_1 C_2} \left(\frac{1}{j\omega} \right) & \omega < \frac{1}{R_1 C_1} \\ -\frac{1}{R_1 C_2} (R_1 C_1) = -\frac{C_1}{C_2} & \omega > \frac{1}{R_1 C_1} \end{cases}$$

$$\frac{C_1}{C_2} = \frac{1}{2}, \frac{1}{R_1 C_1} = 4000 \text{ rad/s}$$



P13.4-13

Pick the appropriate circuit from Table 13.4-2.



$$H(\omega) = -k \frac{1+j\frac{\omega}{z}}{1+j\frac{\omega}{p}}$$

where

$$k = \frac{R_1}{R_2}$$

$$z = \frac{1}{C_1 R_1}$$

$$p = \frac{1}{C_2 R_2}$$

We require

$$200 = z = \frac{1}{C_1 R_1}$$

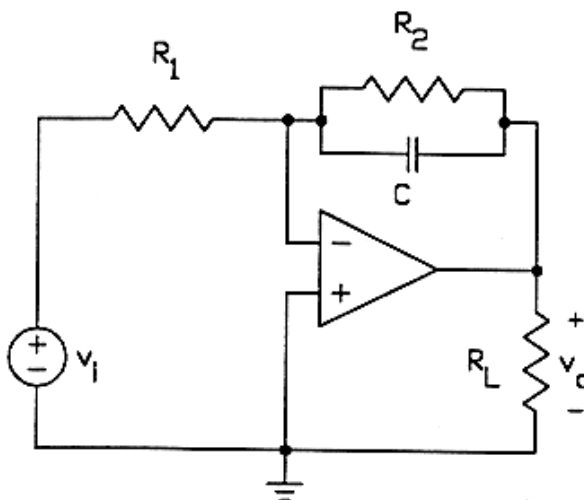
$$500 = p = \frac{1}{C_2 R_2}$$

$$14 \text{ dB} = 5 = k \frac{p}{z} = \frac{C_1}{C_2}$$

Pick $C_1 = 1\mu\text{F}$, then $C_2 = 0.2\mu\text{F}$, $R_1 = 5\text{k}\Omega$ and $R_2 = 10\text{k}\Omega$

P13.4-14

Pick the appropriate circuit from Table 13.4-2.



$$H(\omega) = -\frac{k}{1+j\frac{\omega}{p}}$$

where

$$k = \frac{R_2}{R_1}$$

$$p = \frac{1}{C R_2}$$

We require

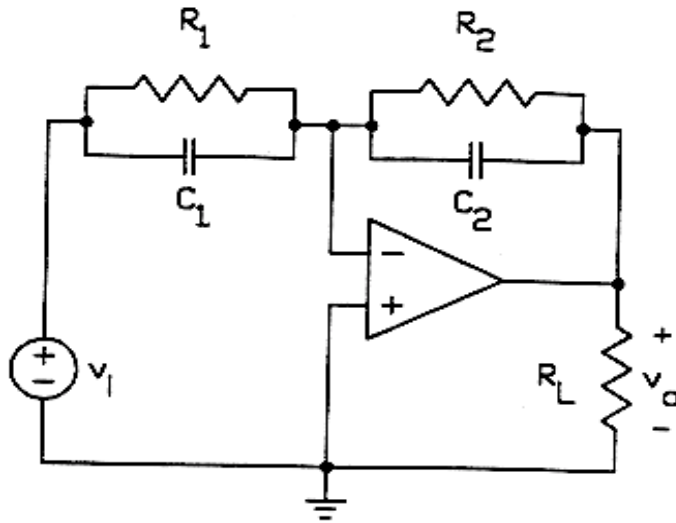
$$500 = p = \frac{1}{C R_2}$$

$$34 \text{ dB} = 50 = \frac{R_2}{R_1}$$

Pick $C = .1\mu\text{F}$, then $R_2 = 20\text{k}\Omega$, $R_1 = 400\Omega$

P13.4-15

Pick the appropriate circuit from Table 13.4-2.



$$H(\omega) = -k \frac{1+j\frac{\omega}{z}}{1+j\frac{\omega}{p}}$$

where

$$k = \frac{R_2}{R_1}$$

$$z = \frac{1}{C_1 R_1}$$

$$p = \frac{1}{C_2 R_2}$$

We require

$$200 = p = \frac{1}{C_2 R_2}$$

$$500 = z = \frac{1}{C_1 R_1}$$

$$14\text{dB} = 5 = k = \frac{R_2}{R_1}$$

Pick $C_1 = 0.1\mu\text{F}$. Then $R_1 = 20\text{k}\Omega$, $R_2 = 100\text{k}\Omega$ and $C_2 = 0.05\mu\text{F}$.